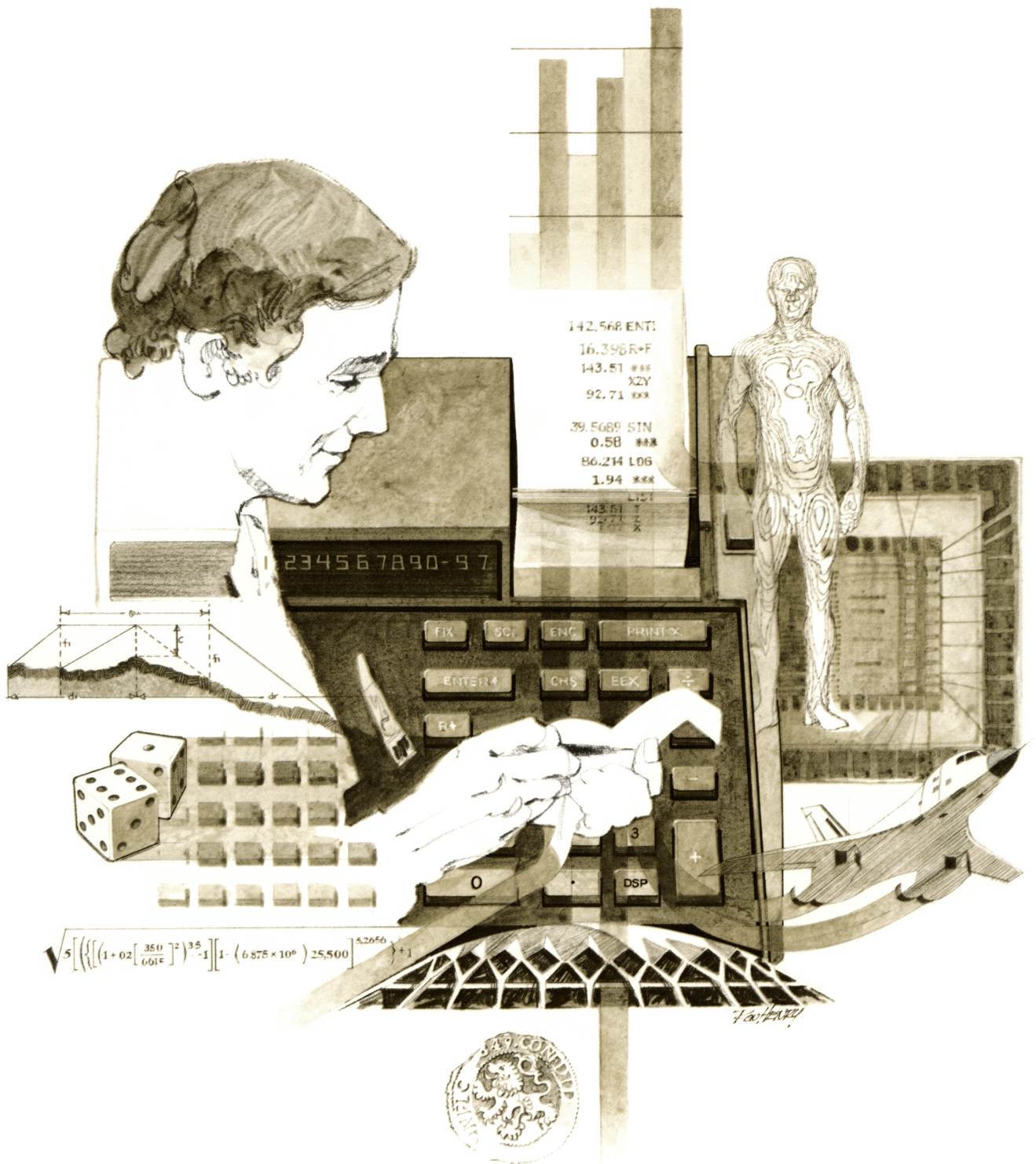


HEWLETT-PACKARD

HP-67/HP-97

Users' Library Solutions

Physics



INTRODUCTION

In an effort to provide continued value to its customers, Hewlett-Packard is introducing a unique service for the HP fully programmable calculator user. This service is designed to save you time and programming effort. As users are aware, Programmable Calculators are capable of delivering tremendous problem solving potential in terms of power and flexibility, but the real genie in the bottle is program solutions. HP's introduction of the first handheld programmable calculator in 1974 immediately led to a request for program **solutions** — hence the beginning of the HP-65 Users' Library. In order to save HP calculator customers time, users wrote their own programs and sent them to the Library for the benefit of other program users. In a short period of time over 5,000 programs were accepted and made available. This overwhelming response indicated the value of the program library and a Users' Library was then established for the HP-67/97 users.

To extend the value of the Users' Library, Hewlett-Packard is introducing a unique service—a service designed to save you time and money. The Users' Library has collected the best programs in the most popular categories from the HP-67/97 and HP-65 Libraries. These programs have been packaged into a series of low-cost books, resulting in substantial savings for our valued HP-67/97 users.

We feel this new software service will extend the capabilities of our programmable calculators and provide a great benefit to our HP-67/97 users.

A WORD ABOUT PROGRAM USAGE

Each program contained herein is reproduced on the standard forms used by the Users' Library. Magnetic cards are not included. The Program Description I page gives a basic description of the program. The Program Description II page provides a sample problem and the keystrokes used to solve it. The User Instructions page contains a description of the keystrokes used to solve problems in general and the options which are available to the user. The Program Listing I and Program Listing II pages list the program steps necessary to operate the calculator. The comments, listed next to the steps, describe the reason for a step or group of steps. Other pertinent information about data register contents, uses of labels and flags and the initial calculator status mode is also found on these pages. Following the directions in your HP-67 or HP-97 **Owners' Handbook and Programming Guide**, "Loading a Program" (page 134, HP-67; page 119, HP-97), key in the program from the Program Listing I and Program Listing II pages. A number at the top of the Program Listing indicates on which calculator the program was written (HP-67 or HP-97). If the calculator indicated differs from the calculator you will be using, consult Appendix E of your **Owner's Handbook** for the corresponding keycodes and keystrokes converting HP-67 to HP-97 keycodes and vice versa. No program conversion is necessary. The HP-67 and HP-97 are totally compatible, but some differences do occur in the keycodes used to represent some of the functions.

A program loaded into the HP-67 or HP-97 is not permanent—once the calculator is turned off, the program will not be retained. You can, however, permanently save any program by recording it on a blank magnetic card, several of which were provided in the Standard Pac that was shipped with your calculator. Consult your **Owner's Handbook** for full instructions. A few points to remember:

The Set Status section indicates the status of flags, angular mode, and display setting. After keying in your program, review the status section and set the conditions as indicated before using or permanently recording the program.

REMEMBER! To save the program permanently, **clip** the corners of the magnetic card once you have recorded the program. This simple step will protect the magnetic card and keep the program from being inadvertently erased.

As a part of HP's continuing effort to provide value to our customers, we hope you will enjoy our newest concept.

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Program Description I

Program Title Black Body Thermal Radiation

Contributor's Name Hewlett-Packard

Address 1000 N. E. Circle Blvd.

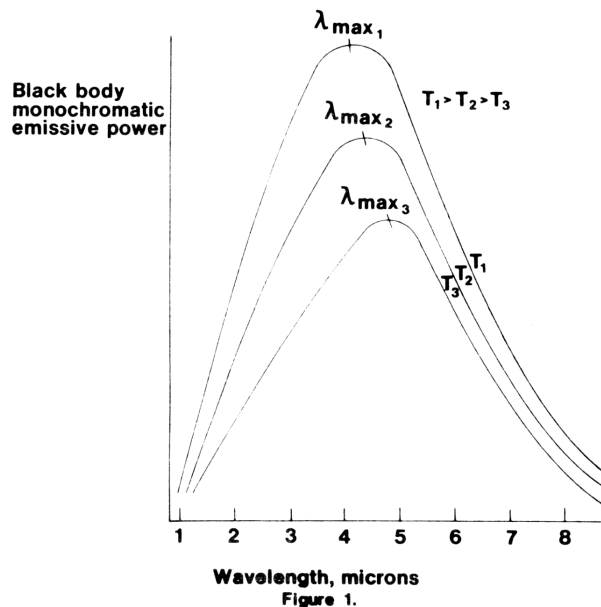
City Corvallis

State Oregon

Zip Code 97330

Program Description, Equations, Variables

Bodies with finite temperatures emit thermal radiation. The higher the absolute temperature, the more thermal radiation emitted. Bodies which emit the maximum possible amount of energy at every wavelength for a specified temperature are said to be black bodies. While black bodies do not actually exist in nature, many surfaces may be assumed to be black for engineering considerations.



(continued next page)

Operating Limits and Warnings

A minute or more may be required to obtain $E_{b(0-\lambda)}$ or $E_{b(\lambda_1-\lambda_2)}$ since the integration is numerical.

Sources differ on values for constants. This could yield small discrepancies between published tables and program outputs.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

NEITHER HP NOR THE CONTRIBUTOR MAKES ANY EXPRESS OR IMPLIED WARRANTY OF ANY KIND WITH REGARD TO THIS PROGRAM MATERIAL, INCLUDING, BUT NOT LIMITED TO, THE IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR PURPOSE. NEITHER HP NOR THE CONTRIBUTOR SHALL BE LIABLE FOR INCIDENTAL OR CONSEQUENTIAL DAMAGES IN CONNECTION WITH OR ARISING OUT OF THE FURNISHING, USE OR PERFORMANCE OF THIS PROGRAM MATERIAL.

Figure 1 is a representation of black body thermal emission as a function of wavelength. Note that as temperature increases, the area under the curves (total emissive power $E_{b(0-\infty)}$) increases. Also note that the wavelength of maximum emissive power $\lambda_{\max}$ shifts to the left as temperature increases.

This program calculates the wavelength of maximum emissive power for a given temperature, the temperature for which a given wavelength would be the wavelength of maximum emissive power, the total emissive power over all wavelengths, the emissive power at a particular wavelength, the emissive power from zero to a specified wavelength, and the emissive power between specified wavelengths.

Equations:

$$\lambda_{\max} T_{\lambda_{\max}} = c_3$$

$$E_{b(0-\infty)} = \sigma T^4$$

$$E_{b\lambda} = \frac{2\pi c_1}{\lambda^5 (e^{c_2/\lambda T} - 1)}$$

$$E_{b(0-\lambda)} = \int_0^{\lambda} E_{b\lambda} d\lambda$$

$$= 2\pi c_1 \sum_{k=1}^{\infty} \frac{1}{k} e^{-k c_2 / \lambda T} \left[\left(\frac{1}{\lambda} \right)^3 + \frac{3T}{\lambda^2 k c_2} + \frac{6}{\lambda} \left(\frac{T}{k c_2} \right)^2 + 6 \left(\frac{T}{k c_2} \right)^3 \right]$$

$$E_{b(\lambda_1 - \lambda_2)} = E_{b(0-\lambda_2)} - E_{b(0-\lambda_1)}$$

where

$\lambda_{\max}$ is the wavelength of maximum emissivity in microns;

T is the absolute temperature in $^{\circ}\text{R}$ or K;

$E_{b(0-\infty)}$ is the total emissive power in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b\lambda}$ is the emissive power at λ in $\text{Btu/hr-ft}^2\text{-}\mu\text{m}$ or $\text{Watts/cm}^2\text{-}\mu\text{m}$;

$E_{b(0-\lambda)}$ is the emissive power for wavelengths less than λ in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b(\lambda_1-\lambda_2)}$ is the emissive power for wavelengths between λ_1 and λ_2 in Btu/hr-ft^2 or Watts/cm^2 .

$$\begin{aligned} c_1 &= 1.8887982 \times 10^7 \text{ Btu-}\mu\text{m}^4/\text{hr-ft}^2 \\ &= 5.9544 \times 10^3 \text{ W}\mu\text{m}^4/\text{cm}^2 \end{aligned}$$

$$c_2 = 2.58984 \times 10^4 \mu\text{m-}^{\circ}\text{R} = 1.4388 \times 10^4 \mu\text{m-K}$$

$$c_3 = 5.216 \times 10^3 \mu\text{m-}^{\circ}\text{R} = 2.8978 \times 10^3 \mu\text{m-K}$$

$$\sigma = 1.713 \times 10^{-9} \text{ Btu/hr-ft}^2\text{-}^{\circ}\text{R}^4 = 5.6693 \times 10^{-12} \text{ W/cm}^2\text{-K}^4$$

$$\sigma_{\text{exp}} = 1.731 \times 10^{-9} \text{ Btu/hr-ft}^2\text{-}^{\circ}\text{R}^4 = 5.729 \times 10^{-12} \text{ W/cm}^2\text{-K}^4$$

Program Description II

Sketch(es)

Sample Problem(s) Example 1:

What percentage of the radiant output of a lamp is in the visible range (0.4 to 0.7 microns) if the filament of the lamp is assumed to be a black body at 2400 K? What is the percentage at 2500 K?

Keystrokes:

Outputs:

[f] [B]-----	→	$5.669 \times 10^{-12} \text{ W/cm}^2\text{-K}^4$
2400 [A] .4 [B] .7 [f] [E] [C] [÷] 100 [x]-----	→	2.641%
2500 [A] .7 [f] [E] [C] [÷] 100 [x]-----	→	3.337%

Example 2:

If the human eye was designed to work most efficiently in sunlight and the visible spectrum runs from about 0.4 to 0.7 microns, what is the sun's temperature in degrees Rankine? Assume that the sun is a black body. Using the temperature calculated, find the fraction of the sun's total emissive power which falls in the visible range. Find the percentage of the sun's radiation which has a wavelength less than 0.4 microns.

Keystrokes:

Outputs:

[f] [A]-----	→	$1.713 \times 10^{-9} \text{ Btu/hr-ft}^2\text{-}^\circ\text{R}^4$
Compute mean of visible range.		
.4 [+] .7 [+] 2 [÷]-----	→	$550.0 \times 10^{-3} \mu\text{m}$
Compute temperature of sun.		
[B]-----	→	$9.484 \times 10^3 \text{ }^\circ\text{R}$
(continued)		

Reference(s)

Robert Siegel and John R. Howell, *Thermal Radiation Heat Transfer*,
Volume 1, National Aeronautics and Space Administration, 1968.

Compute percentage of power in visible range.

[A] .4 [B] .7 [E] [C] [÷] 100 [x]-----→ $33.70 \times 10^0 \%$

Compute percentage of power under 0.4 microns.

[E] [C] [÷] 100 [x]-----→ **8.433%**

Black Body Thermal Radiation

Eng	SI	Exp	σ	$\lambda' \rightarrow$
$T \rightarrow \lambda_{\max}$	$\lambda \rightarrow T(\lambda_{\max})$	$\rightarrow E_b(0-\infty)$	$\rightarrow E_{b\lambda}$	$E_b(\lambda-\lambda')$ $E_b(0-\lambda)$

[illegible]

97Program Listing I

7

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBL0	21 16 11	Store English constants.	057	5	05	
002	1	01		058	.	-62	
003	0	08		059	6	06	
004	0	08		060	6	06	
005	0	08		061	9	09	
006	7	07		062	3	03	
007	9	09		063	EEX	-23	
008	0	08		064	CHS	-22	
009	2	02		065	1	01	
010	ST01	35 01		066	2	02	
011	2	02		067	ST04	35 04	
012	5	05		068	RTN	24	
013	0	08		069	*LBL0	21 16 13	Convert to experimental σ .
014	9	09		070	1	01	
015	0	08		071	.	-62	
016	.	-62		072	0	00	
017	4	04		073	1	01	
018	ST02	35 02		074	0	00	
019	5	05		075	5	05	
020	2	02		076	ST*4	35-35 04	
021	1	01		077	RCL4	36 04	
022	6	06		078	RTN	24	
023	ST03	35 03		079	*LBLA	21 11	
024	.	-62		080	ST05	35 05	
025	1	01		081	RCL3	36 03	
026	7	07		082	X*Y	-41	
027	1	01		083	=	-24	
028	3	03	Store SI constants.	084	RTN	24	Store λ and calculate T for which λ would be $\lambda_{\max}$.
029	1	01		085	*LBLB	21 12	
030	2	02		086	ST06	35 06	
031	EEX	-23		087	RCL3	36 03	
032	CHS	-22		088	X*Y	-41	
033	0	08		089	=	-24	
034	ST04	35 04		090	RTN	24	
035	RTN	24		091	*LBLC	21 13	
036	*LBL0	21 16 12		092	RCL5	36 05	Calculate $E_{b(0-\infty)}$.
037	5	05		093	X^2	53	
038	9	09		094	X^2	53	
039	5	05		095	RCL4	36 04	
040	4	04		096	X	-35	
041	.	-62		097	RTN	24	
042	4	04		098	*LBLD	21 14	
043	ST01	35 01		099	RCL1	36 01	
044	1	01		100	ENT1	-21	
045	4	04		101	+	-55	
046	3	03		102	Pi	16-24	
047	0	08		103	X	-35	
048	0	08		104	RCL6	36 06	
049	ST02	35 02		105	5	05	Calculate $E_{b\lambda}$.
050	2	02		106	Y*	31	
051	0	08		107	=	-24	
052	9	09		108	RCL2	36 02	
053	7	07		109	RCL6	36 06	
054	.	-62		110	=	-24	
055	0	08		111	RCL5	36 05	
056	ST03	35 03		112	=	-24	

REGISTERS

0	1	2	3	4	5	6	7	8	9
λ	C_1	C_2	C_3	σ	T	λ, λ'	sum	kc_2/T	
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C	D	E	I				

97 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	e ^x	33		169	X $\leftrightarrow$ Y?	16-35	
114	1	01		170	GT01	22 01	
115	-	-45		171	R $\downarrow$	-31	
116	$\div$	-24		172	CLX	-51	
117	RTN	24		173	RCL7	36 07	
118	*LBL $\bar{E}$	21 15	Calculate $E_{b(0-\lambda)}$.	174	ENT $\uparrow$	-21	
119	0	00		175	+	-55	
120	ST08	35 08		176	Pi	16-24	
121	ST07	35 07		177	$\times$	-35	
122	*LBL1	21 01		178	RCL1	36 01	
123	R $\downarrow$	-31		179	$\times$	-35	
124	CLX	-51		180	RTN	24	
125	RCL8	36 08		181	*LBL $\bar{e}$	21 16 15	Calculate $E_{b(\lambda-\lambda')}$.
126	RCL2	36 02		182	ENT $\uparrow$	-21	
127	RCL5	36 05		183	ENT $\uparrow$	-21	
128	$\div$	-24		184	GSBE	23 15	
129	-	-45		185	X $\leftrightarrow$ Y	-41	
130	ST08	35 08		186	RCL6	36 06	
131	3	03		187	ST00	35 00	
132	X $\leftrightarrow$ Y	-41		188	R $\downarrow$	-31	
133	$\div$	-24		189	ST06	35 06	
134	RCL6	36 06		190	GSBE	23 15	
135	X $\leftrightarrow$	53		191	-	-45	
136	$\div$	-24		192	ABS	16 31	
137	LSTX	16-63		193	RCL0	36 00	
138	1/X	52		194	ST06	35 06	
139	RCL6	36 06		195	R $\downarrow$	-31	
140	$\div$	-24		196	RTN	24	
141	-	-45					
142	6	06					
143	RCL6	36 06		200			
144	$\div$	-24					
145	RCL8	36 08					
146	X $\leftrightarrow$	53					
147	$\div$	-24					
148	-	-45					
149	6	06					
150	RCL8	36 08					
151	X $\leftrightarrow$	53					
152	$\div$	-24					
153	RCL8	36 08		210			
154	$\div$	-24					
155	+	-55					
156	RCL8	36 08					
157	RCL6	36 06					
158	$\div$	-24					
159	e ^x	33					
160	$\times$	-35					
161	RCL8	36 08					
162	$\div$	-24					
163	ST+7	35-55 07					
164	RCL7	36 07		220			
165	$\div$	-24					
166	EE $\times$	-23					
167	CHS	-22					
168	5	05					

LABELS					FLAGS	SET STATUS		
A $T \rightarrow \lambda$	B $\lambda \rightarrow T(\lambda_{\max})$	C $\rightarrow E_{b(0-\infty)}$	D $\rightarrow E_{b-\lambda}$	E $\rightarrow E_{b(0-\lambda)}$	0	ON OFF		
a Eng	b SI	c Exp σ	d	e $\lambda' \rightarrow E_{b(\lambda-\lambda')}$	1	FLAGS		
0	1 $E_{b(0-\lambda)}$	2	3	4	2	DEG ☒	TRIG ☒	DISP ☐
5	6	7	8	9	3	GRAD ☐	SCI ☐	ENG ☒
						RAD ☐		n <u>3</u>

Program Description I

Program Title *Black Hole Characteristics*

Contributor's Name *Geoff Kidd*

Address *1514 Oxford St #301*

City *Berkeley*

State *CA*

Zip Code *94709*

Program Description, Equations, Variables

A black hole of mass (M) in grams has a Schwarzschild radius (R_s) in centimeters of:

$R_s = \frac{2GM}{c^2} = (M) \cdot 1.484986855 \times 10^{-28}$ where G is the universal gravitational constant and c is the speed of light.

The lifetime of a black hole (t_L) in seconds is given by:

$$t_L = M^3 \cdot (10^{-28}).$$

The temperature of a black hole (K) in degrees Kelvin is

$$K = 10^{26}/M$$

Operating Limits and Warnings *M must be greater than zero*

Underflow occurs for R_s when $M < 6.734066343 \times 10^{-72}$
 t_L $M < 2.154434653 \times 10^{-24}$

Overflow occurs for K when $M < 1.000000001 \times 10^{-74}$
 t_L $M > 2.154434650 \times 10^{33}$
 M $R_s > 1.484986854 \times 10^{72}$

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s)

- 1.) The sun has a mass 1.99×10^{33} gm. What would be the temperature, Schwarzschild radius, and lifetime of a black hole of that mass?
- 2.) Given a Schwarzschild radius of 6.96×10^{10} cm, what is the mass of the black hole? What is the temperature?

Solution(s)

1.) 1.99 EEX 33 D $\rightarrow 1.9900 \times 10^{33}$
A $\rightarrow 2.9551 \times 10^5$ r_s
B $\rightarrow 5.0251 \times 10^8$ K
C $\rightarrow 7.8806 \times 10^{71}$ t_L

2.) 6.96 EEX 10 A $\rightarrow 6.9600 \times 10^{10}$
D $\rightarrow 4.6869 \times 10^{38}$ M
B $\rightarrow 2.1336 \times 10^{-13}$ K

Reference(s) Horwitt, Martin Astrophysical Concepts Wiley, New York

User Instructions

A diagram of a black hole represented as a horizontal rectangle with a thick black border. Inside the rectangle, the text "BLACK HOLE CHARACTERISTICS" is written in all caps. Below this text, four symbols are spaced out: R_s , K , t_L , and M . On the left side of the rectangle, there is a small black triangle pointing left, labeled "1", and a small square icon with the letters "CP" inside. On the right side, there is a small black triangle pointing right, labeled "2".

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS		OUTPUT DATA/UNITS
1.	Enter program				
2.	Enter mass	M	D		m
	or Schwarzschild radius	R _s	A		R _s
	or temperature	K	B		K
	or lifetime	t _L	C		t _L
3.	Compute mass		D		m
	or Schwarzschild radius		A		R _s
	or Temperature		B		K
	or lifetime		C		t _L
	For a different variable, go to 3				
	For a new case, go to 2				
	Before any computations, at least one of the four variables must have been entered or results will be unpredictable				
	Note: a new value <u>entered</u> for R _s , t _L or K causes the mass stored in memory to be recalculated.				

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS											
001	LBL A	31 25 11	Schwarzschild Radius $R_s =$ $M \cdot$ $1.484986855 \times 10^{-28}$		6	06	$M = \frac{10^{26}}{K}$ Lifetime $t_L = M^3 \cdot 10^{-28}$											
	R F? 3	35 71 03			R XZy	35 52												
	GT0 0	22 00			÷	81												
	1	01		060	ST0 3	33 03												
	.	83			RCL 1	34 01												
	4	04			R RTN	35 22												
	8	08			LBL C	31 25 13												
	4	04			R F? 3	35 71 03												
	9	09			GT0 0	22 00												
010	8	08			EEX	43												
	6	06	Entered value of R_s , compute new mass $M =$ $R_s \cdot 6.734066344$ $\times 10^{27}$		CHS	42	Entered value of t_L , compute new mass $M = \sqrt[3]{t_L \cdot 10^{28}}$											
	8	08			2	02												
	5	05			8	08												
	5	05		070	RCL 3	34 03												
	EEX	43			EM	41												
	2	02			3	03												
	8	08			R yx	35 63												
	CHS	42			XV	71												
	RCL 3	34 03			ST0 2	33 02												
020	X	71			R RTN	35 22												
	ST0 0	33 00	Entered value of R_s , compute new mass $M =$ $R_s \cdot 6.734066344$ $\times 10^{27}$		LBL 0	31 25 00	Entered value of t_L , compute new mass $M = \sqrt[3]{t_L \cdot 10^{28}}$											
	R RTN	35 22			ST0 2	33 02												
	LBL 0	31 25 00			EEX	43												
	ST0 0	33 00		080	2	02												
	6	06			8	08												
	.	83			X	71												
	7	07			3	03												
	3	03			R 1/x	35 62												
	4	04			R 4/x	35 63												
030	0	00			ST0 3	33 03												
	6	06	Entered value of R_s , compute new mass $M =$ $R_s \cdot 6.734066344$ $\times 10^{27}$		RCL 2	34 02	Mass If new value not entered, display old. Else store value entered.											
	6	06			R RTN	35 22												
	3	03		090	LBL D	31 25 14												
	4	04			R F? 3	35 71 03												
	4	04			GT0 0	22 00												
	EEX	43			RCL 3	34 03												
	2	02			R RTN	35 22												
	7	07			LBL 0	31 25 00												
	X	71			ST0 3	33 03												
040	ST0 3	33 03			R RTN	35 22												
	RCL 0	34 00	Temperature $K = 10^{26}/M$		R/S	84	Flag 0-4 off deg mode SCI DSP 4 are initial values Labels used: A, B, C, D, O											
	R RTN	35 22		100														
	LBL B	31 25 12																
	R F? 3	35 71 03																
	GT0 0	22 00																
	EEX	43																
	2	02																
	6	06																
	RCL 3	34 03																
050	÷	81																
	ST0 1	33 01	Entered value of K , compute new Mass	110														
	R RTN	35 22																
	LBL 0	31 25 00																
	ST0 1	33 01																
	EEX	43																
	2	02																
REGISTERS																		
0	R _s	1	K	2	t _L	3	M	4		5		6		7		8		9
S0		S1		S2		S3		S4		S5		S6		S7		S8		S9
A		B		C		D		E		F		G		H		I		J

Program Description I

Program Title SPECIAL RELATIVITY CONVERSIONS

Contributor's Name Ctein

Address 298 Vista Grande

City Daly City

State Ca

Zip Code 94014

Program Description, Equations, Variables This program provides relativistic conversions between the following quantities: rest mass (m); velocity (v , in units of $c=1$); energy (E), and momentum (P). Given any two it is possible to find the two unknowns by the following equations:

(I)-- $E = m/\text{SQRT}(1-v^2)$ // (II)-- $E = \text{SQRT}(P^2 + m^2)$ // (III)-- $E = P/v$

(IV)-- $P = vE$ // (V)-- $P = \text{SQRT}(E^2 - m^2)$ // (VI)-- $v = P/E$ // (VII) $m = \text{SQRT}(E^2 - P^2)$

Data may be entered in any order and recalled at any time. The program scans the registers and, after determining if there is enough data to solve for the unknown, selects the appropriate subset of equations. If insufficient data, then the program displays Error. The following selection patterns are used:

TO FIND:	v	m	E	P
GIVEN:	m, E	v, E	v, m	v, E
	use V, VI	use IV, VII	use I	use IV
	m, P	v, P	v, P	v, m
	use II, VI	use III, VII	use III	use I, IV
	E, P	E, P	m, P	m, E
	use VI	use VII	use II	use V

Because of the complexity of this program, a chart is provided on the next page which diagrams the access patterns used by each labeled subsection. Boxes are used to represent direct jumps, and circles represent subroutine calls. The user is advised to review this carefully before modifying this program.

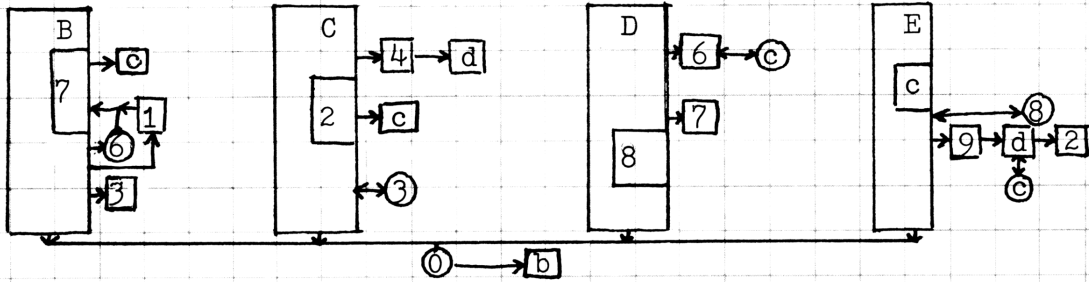
Operating Limits and Warnings

all data must be positive. Velocity must be less than 1. ERROR message will be displayed if a real solution does not exist or the input data is outside these limits.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Special Relativity



Sample Problem(s)

- ### Sample Problem(s)

Solution(s)

- Solution(s)**

Reference(s) HP-65 library program #308 by this author.

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[illegible]

67 Program Listing I

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS		
001	*LBL A	31 25 11	RESET		*LBL 8	31 25 08	v in X		
	CL REG	31 43			x←y	35 52			
	CF 3	35 61 03			asin	32 62	SQRT(1-v ²)		
	R/S	84		060	cos	31 63			
	*LBL B	31 25 12	FIND/STORE v		/	81	eq.I gives E		
	1	01			RTN	35 22			
	GSB 0	31 22 00	store new v		*LBL E	31 25 15	FIND/STORE P		
	RCL 2	34 02	m		4	04			
	x=0?	31 51	if m is unknown		GSB 0	31 22 00	store new P		
010	GTO 1	22 01	then go to 1		x=0?	31 51	if v is unknown		
	RCL 3	34 03	E		GTO 9	22 09	then go to 9.		
	x≠0?	31 61	if E,m are known		RCL 2	34 02	if m,v known,		
	GTO 3	22 03	then go to 3		x≠0?	31 61	then eq.I gives		
	GSB 6	31 22 06	eq.II gives E	070	GSB 8	31 22 08	E.		
	ENTER	41			RCL 3	34 03	If R ₃ contains		
	*LBL 7	31 25 07			x=0?	31 51	E(i.e.≠0), then		
	R ↓	35 53			R ↓	35 53	this takes prior		
	RCL 4	34 04	P		RCL 1	34 01	ity.		
	x←y	35 52	E		x	71	eq.IV gives P		
020	/	81	eq. VI gives v		*LBL c	32 25 13	-----		
	GTO c	22 31 13	check out P		x=0?	31 51	if variable or		
	*LBL C	31 25 13	FIND/STORE m		/	81	result is not		
	2	02			RTN	35 22	legitimate,end.		
	GSB 0	31 22 00	store new m	080	*LBL 0	31 25 00	check/store 'x'		
	x=0?	31 51	if v is unknown		ST I	35 33	store (i)		
	GTO 4	22 04	then go to 4		F? 3	35 71 03	if data has been		
	RCL 3	34 03	E		GTO b	22 31 12	entered,go to b		
	x	71	eq.IV gives P		RCL(i)	34 24	check contents		
	LST x	35 82	E		x≠0?	31 61	of register 'x'		
030	x≠0?	31 61	if E is known,		R/S	84	and display if		
	GTO 2	22 02	go to 2		RCL 1	34 01	good. Otherwise		
	RCL 4	34 04	P		RTN	35 22	RCL v and return		
	ENTER	41			*LBL b	32 25 12	STORE NEW "x"		
	ENTER	41		090	R ↓	35 53	in register defi		
	RCL 1	34 01	v		STO(i)	33 24	ned by (i)		
	/	81	eq.III gives E		R/S	84			
	*LBL 2	31 25 02	eq. V or VII		*LBL 1	31 25 01	FIND v;m UNKNOWN		
	ENTER	41			RCL 3	34 03	E		
	R ↓	35 53			ENTER	41			
040	GSB 3	31 22 03	SQRT(x ² -y ²)		GTO 7	22 07	eq.VI gives v		
	R ↑	35 54			*LBL 4	31 25 04	FIND m;v UNKNOWN		
	x	71	eq.VII gives m		RCL 4	34 04	P		
	GTO c	22 31 13	check for valid		GTO d	22 31 14	go to d		
	*LBL 3	31 25 03	results	100	*LBL 6	31 25 06	EQ. II		
	/	81	find		RCL 2	34 02	m		
	asin	32 62	SQRT(1-y ² /x ²)		GSB c	32 22 13	check validity		
	cos	31 63			RCL 4	34 04	P		
	RTN	35 22			GSB c	32 22 13	check validity		
	*LBL D	31 25 14	FIND/STORE E		R→P	32 72	E=SQRT(m ² +P ²)		
050	3	03			RTN	35 22			
	GSB 0	31 22 00	store new E		*LBL 9	31 25 09	FIND P:v UNKNOWN		
	x=0?	31 51	if v is unknown		RCL 2	34 02	m		
	GTO 6	22 06	then go to 6.		*LBL d	32 25 14	-----		
	RCL 2	34 02	if m is unknown	110	GSB c	32 22 13	check validity		
	x=0?	31 51	then go to 7.		RCL 3	34 03	E		
	GTO 7	22 07			GTO 2	22 02	eq.V orVII		
REGISTERS									
0	1	2	3	4	5	6	7	8	9
	velocity	mass	energy	momentum					
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C	D	E	I				used

Program Description I

Program Title Three Dimensional Special Relativity

Contributor's Name William C. Wickes

Address Princeton University, Department of Physics

City Princeton

State N.J.

Zip Code 08540

Program Description, Equations, Variables

1. Given the components of any 4-vector, in particular

$x'^{\mu} = (x', y', z', ct')$ or $p'^{\mu} = (p'^x, p'^y, p'^z, E')$, calculate the components x^{μ} or p^{μ} in a frame in which the original frame^C is moving with velocity $\vec{\beta} = (\beta^x, \beta^y, \beta^z, .)$.

$\vec{p}$ = momentum

E = total energy

$\vec{\beta} = \vec{v}/c$ $\vec{v}$ = velocity

2. For any $\vec{\beta}$, calculate the time-dilation/length contraction factor γ .

3. For a 4-vector Δx^{μ} connecting any two space-time events, calculate the invariant interval $c\Delta\tau$.

Formulae:

$$\Delta\vec{x} = \Delta\vec{x}' + \vec{\beta}[(\gamma-1) \frac{\vec{\beta} \cdot \vec{x}'}{\beta^2} + \gamma c\Delta t']$$

$$\Delta t = \gamma(t + \vec{\beta} \cdot \vec{x}/c^2)$$

$$\gamma = [1 - \beta^2]^{-1/2}$$

$$\beta = |\vec{\beta}| = [\beta^x^2 + \beta^y^2 + \beta^z^2]^{1/2}$$

$$|\Delta\vec{x}| = [\Delta x^2 + \Delta y^2 + \Delta z^2]^{1/2}$$

$$c^2\Delta\tau^2 = c^2\Delta t^2 - |\Delta\vec{x}|^2$$

The coordinate frames are assumed to be synchronized so that the event (0,0,0,0) has the same coordinates in both frames.

Operating Limits and Warnings For a spacelike interval, $c^2\Delta\tau^2 < 0$, the calculator will display " - |c\Delta\tau|"

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

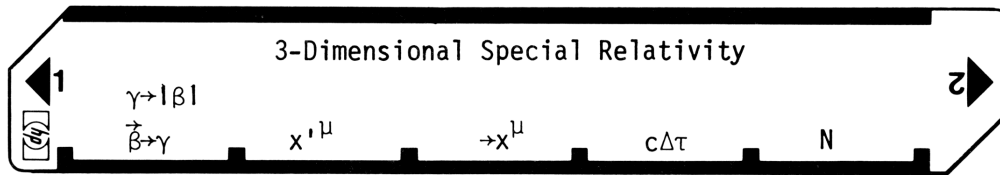
Sketch(es)

Sample Problem(s) An observer moving relative to the Earth with velocity $\vec{\beta} = (.4, .5, .6)$ measures the coordinates of an event as $x'^{\mu} = (1, 2, 3, 4)$.

- Give the coordinates relative to the Earth frame.
- What is the interval between the event and the origin $(0,0,0,0)$

```
Solution(s)      (If necessary) Set dimensions = 3:  3[E] -----3.00
Enter β̄: .4[↑] .5[↑] .6[A] ----- .88*** |β̄|
                                           2.09    γ
Enter x'μ: 1[↑] 2[↑] 3[↑] 4[B] ----- 1.00    x'
Calculate cΔτ           [D] ----- 1.41    cΔτ
Calculate xμ:           [C] -----15.01*** t
                                           10.71*** z
                                           8.43*** y
                                           6.14*** x
```

Reference(s) J.D. Jackson, Classical Electrodynamics (J. Wiley & Sons, NY 1962)



STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS		OUTPUT DATA/UNITS
1.	Set number space dimensions N (default is N=3)	1,2,or 3		E	N
2.	Enter $\vec{\beta}$ (if N=3) (if N>1)	β^x β^y β^z			
			A		β^{***}
					γ
3.	Enter x^μ , (if N=3) (if N>1)	x y z ct			
			B		x
4.	Compute x^μ		C		$x^{***}(\text{if } N=3)$
					$y^{***}(\text{if } N>1)$
					z^{***}
					ct
5.	Compute $c\Delta\tau$ Result is positive if $c\Delta\tau$ negative if $-c\Delta\tau$		D		$\pm c\Delta\tau $
6.	To calculate the speed β corresponding to a dilation factor γ	γ	f	A	β

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS				
001	LBL D	31 25 14	Compute $\sum x_i^2$		LST X	35 82	$1/\beta$ ----- $\sqrt{1-\beta^2}$ γ DISPLAY β ----- STO β				
	RCL 6	34 06			STO 1	33 01					
	F? 0	35 71 00			X $\neq$ y	35 52					
	GTO 4	22 04		060	F? 1	35 71 01					
	RCL 4	34 04			GTO 6	22 06					
	R $\rightarrow$ P	32 72			R $\uparrow$	35 54					
	F? 1	35 71 01			STO 2	33 02					
	GTO 4	22 04			R $\rightarrow$ P	32 72					
	RCL 5	34 05			LBL 6	31 25 06					
	R $\rightarrow$ P	32 72			STO A	33 11					
010	LBL 4	31 25 04	$c^2x^2 - x^2$ ----- SPACE LIKE? SFO ----- - for SPACE LIKE ----- Calculate β from γ		COS $^{-1}$	32 63	γ $\beta \cdot x^i$ ----- $x^{1/2} \rightarrow x^{1/4}$ $\beta \cdot x^i$				
	X 2	32 54			SIN	31 62					
	RCL 7	34 07			1/X	35 62					
	X 2	32 54		070	STO B	33 12					
	-	51			RCL A	34 11					
	CHS	42			-X-	31 84					
	X < 0	31 71			X $\neq$ y	35 52					
	SFO	35 51 02			RTN	35 22					
	ABS	35 64			LBL B	31 25 12					
	$\sqrt{x}$	31 54			STO 7	33 07					
020	F? 2	35 71 02	- for SPACE LIKE ----- Calculate β from γ		R $\downarrow$	35 53	STO β				
	CHS	42			STO 6	33 06					
	RTN	35 22			R $\downarrow$	35 53					
	LBL Q	32 25 11		080	STO 4	33 04					
	STO B	33 12			R $\downarrow$	35 53					
	X 2	32 54			STO 5	33 05					
	1/X	35 62			RTN	35 22					
	1	01			LBL C	31 25 13					
	-	51			GSB E	32 22 15					
	CHS	42			RCL A	34 11					
030	$\sqrt{x}$	31 54	Compute $\beta \cdot x^i$ $= \sum_i \beta^i x^i$		X 2	32 54	USE R0 AS COUNTER Compute one component each cycle				
	STO A	33 11			$\div$	81					
	RTN	35 22			RCL B	34 12					
	LBL E	32 25 15		090	1	01					
	RCL 6	34 06			-	51					
	RCL 3	34 03			X	71					
	X	71			RCL B	34 12					
	F? 3	35 71 00			RCL 7	34 07					
	RTN	35 22			X	71					
	RCL 1	34 01			+	61					
040	RCL 4	34 04	Compute γ		STO C	33 13	USE R0 AS COUNTER Compute one component each cycle				
	X	71			3	03					
	+	61			STO 0	33 00					
	F? 1	35 71 01		100	ST I	35 33					
	RTN	35 22			LBL O	31 25 00					
	RCL 2	34 02			RCL O	34 00					
	RCL 5	34 05			ST I	35 33					
	X	71			RCL C	34 13					
	+	61			RCL (1)	34 24					
	RTN	35 22			X	71					
050	LBL A	31 25 11	Compute γ		RCL I	35 34	USE R0 AS COUNTER Compute one component each cycle				
	STO 3	33 03			3	03					
	F? 0	35 71 00			+	61					
	GTO 6	22 06		110	ST I	35 33					
	X $\neq$ y	35 52			CLX	44					
	R $\rightarrow$ P	32 72			RCL (1)	34 24					
REGISTERS											
0 Counter	1 β^4	2 β^2		3 β^3	4 γ	5 x		6 β	7 ct	8	9
S0	S1	S2		S3	S4 γ'	S5 x'		S6 β'	S7 ct'	S8	S9
A β	B γ	C		D	E	I USED					

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[illegible]

Program Description I

Program Title Einsteins Twin Paradox
Contributor's Name David M. Weingold
Address % Synergy Research P.O. Box 372
City Woodmere **State** N.Y. **Zip Code** 11598

Program Description, Equations, Variables

The program is arranged to calculate subjective and real time differential between an observer on Earth and the pilot of a vehicle accelerating near the speed of light. If you imagine twins at age 21. One becomes an astronaut and volunteers for the first interstellar flight. He takes off and travels at a ponderous speed of say 2.994444444×10^8 meters per second. In this situation it is accurate enough to call C the speed of light, 3×10^8 . The astronaut travels for what he measures to be a year well past the sun at which time he fires retro and navigational engines, and turns around and heads toward Earth; the journey naturally takes another year. He is now 23 years old but when he steps from the ship his twin is over 37 years old! That over 16 years had passed on Earth. The explanation as to why this happened involves very complicated non Euclidian geometry and relativistic considerations of accelerating frame of reference too complicated for this discussion, it suffices to say that in the event of tremendous accelerations such as the turning around of a space craft traveling near the speed of light that the order of magnitude of energy involved is extremely large and the consideration of it as it interrelates to space as time is conceived as a fourth physical

Operating Limits and Warnings

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Program Description I

Program Title Einsteins Twin Paradox

Contributor's Name David M. Weingold

Address % Synergy Research P.O. Box 372

City Woodmere

State New York

Zip Code 11598

Program Description, Equations, Variables

dimension of space, the Universe is then conceived as a giant four dimensional sphere with a three dimensional surface. The space craft in its turning travels relative to the Earth, not as far along that fourth dimension and hence the differential between the twins age. The equations for this case are quite simple and adequate for this case. They consist primarily of the Lorentz transform i.e., $\sqrt{1 - \frac{v^2}{c^2}}$, where v is the velocity of the space craft relative to the Earth, and c is the universal constant, 3×10^8 meters per second, the speed of light. The program inputs consist of speed of space craft in meters per second, time passed on Earth, time passed on board the craft, and the ages of the twins before the flights. With input T_E , time passed on Earth, the equation $T_S = T_E \sqrt{1 - \frac{v^2}{c^2}}$ gives T_S , ["time passed on board"] ship during journey. Input T_S , time passed on board ship, and the equation: $T_E = \frac{T_S}{\sqrt{1 - \frac{v^2}{c^2}}}$ gives you T_E , ["time passed on Earth"] during journey. The label A clears and initiates the program. Lbl B is the input for average velocity of the craft. Lbl C is the input for time passed on earth in years and outputs time passed on board ship by hitting fC Lbl D input time passed on board ship fD give appropriate time passed on earth the E's give ages.

Operating Limits and Warnings

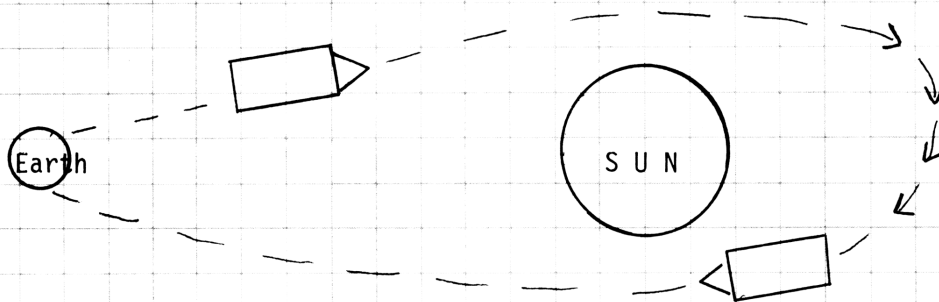
Be certain that you enter the speed of the space craft in meters per second. All time and age entries must be in years. Outputs will be in years. Do not try to make the space travel at the speed of light, $\approx (3.00 \times 10^8 \text{ meters/second})$ as this will only show an error as should be and is implied by the theory of relativity.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)



Sample Problem(s) Suppose two twins, age thirty, take part in this experiment the velocity of the ship will average 2.999111111×10^8 , if the twin on board travels a total of one year how much time will have passed on Earth? And given that 25 years passes on earth before return of the ship, how much time passed on board? What was the age differential in both cases?

Solution(s) Load side 1 and side 2
 [A] -----> -9.00×10^{16}
 2.999111111 [EEX] 8 [B]
 1 [D] [f] [D] -----> 41.08 years passed on Earth
 30 [E] -----> 71 twin on Earth's age
 Age differential is 40 years (71-31)
 [A]
 2.999111111 [EEX] 8 [B]
 25 [C] [f] [C] -----> .6085 years passed in space

30 [f] [E] -----> 30.6085 twin on board's age
 Age differential is 24.3015 (55-30.6085)

REFERENCE (S) Introduction to Special Relativity by James H. Smith (chp. 6)
 W.A. Benjam Inc., New York, Amsterdam 1965.

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[illegible]

97 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	X	-35	
002	CLRG	16-53		058	RCL1	36 01	Enter Time
003	SCI	-12		059	X	-35	Passed in Space
004	DSP9	-63 09		060	RCL2	36 02	Convert from
005	CLX	-51		061	X	-35	Years To Seconds
006	3	03		062	STOD	35 14	Store in RD
007	6	06		063	RTN	24	
008	0	00		064	*LBLd	21 16 14	
009	0	00		065	RCLD	36 14	
010	STO0	35 00		066	GSB0	23 00	
011	2	02		067	+	-24	
012	4	04		068	RCL0	36 00	
013	STO1	35 01		069	+	-24	
014	3	03		070	RCL1	36 01	
015	6	06		071	+	-24	
016	5	05		072	RCL2	36 02	
017	.	-62		073	+	-24	
018	2	02		074	STO4	35 04	
019	5	05		075	PSE	16 51	
020	STO2	35 02		076	SPC	16-11	
021	3	03		077	PRTX	-14	
022	EEX	-23		078	RTN	24	
023	28	08		079	*LBL0	21 00	
024	X	53		080	RCLB	36 12	
025	STOA	35 11		081	RCLA	36 11	
026	RTN	24		082	+	-24	
027	*LBLB	21 12		083	CHS	-22	
028	X ²	53		084	1	01	
029	STOB	35 12		085	+	-55	
030	RTN	24		086	√X	54	
031	*LBLC	21 13		087	RTN	24	
032	RCL0	36 00		088	*LBL E	21 15	
033	X	-35		089	RCL4	36 04	
034	RCL1	36 01		090	+	-55	
035	X	-35		091	PSE	16 51	
036	RCL2	36 02		092	SPC	16-11	
037	X	-35		093	PRTX	-14	
038	STOC	35 13		094	RTN	24	
039	RTN	24		095	*LBL e	21 16 15	
040	*LBLc	21 16 13		096	RCL3	36 03	
041	RCLC	36 13		097	+	-55	
042	GSB0	23 00		098	PSE	16 51	
043	X	-35		099	SPC	16-11	
044	RCL0	36 00		100	PRTX	-14	
045	÷	-24		101	RTN	24	
046	RCL1	36 01			R/S	51	
047	+	-24					
048	RCL2	36 02					
049	+	-24					
050	STO3	35 03					
051	PSE	16 51					
052	SPC	16-11					
053	PRTX	-14					
054	RTN	24					
055	*LBLD	21 14					
056	RCL0	36 00					

initiate
store constants
clear registers
find C² and store
in RA.

Enter ship Avg. Velocity
square and store
in RB

Enter Time Passed
on Earth in years
convert to seconds
store in RC

Calculate
 $T_s = T_e \sqrt{1 - \frac{v^2}{c^2}}$
store R3
space and print

Enter Time
Passed in Space
Convert from
Years To Seconds
Store in RD

Calculate
 $T_e = \frac{T_s}{\sqrt{1 - \frac{v^2}{c^2}}}$
Store in R4

subroutine
 $\sqrt{1 - \frac{v^2}{c^2}}$

Calculate
Earth Twin Final
Age

Calculate space
Twin Final age

REGISTERS									
0 3600	1 24	2 365.25	3 T _s	4 T _e	5	6	7	8	9
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C time passed Earth in sec.	D time passed rocket in sec.	E	F	G	H	I	J

Program Description I

Program Title **Delta-V - Orbit Simulator**

Contributor's Name **Harold T. Coderre**

Address **414 1915 Hall**

City **Princeton**

State **New Jersey**

Zip Code **08540**

Program Description, Equations, Variables This program calculates orbit parameters from initial position and velocity data both for elliptical and hyperbolic orbits in a plane. It is also possible to move the point of interest to anywhere along the orbit and then recalculate orbit parameters.

Equations Used:

$$\text{Energy: } E = \frac{1}{2} V_i^2 - \frac{GM}{R_i}$$

$$\text{Angular Momentum: } L = v r \sin(\alpha_i - \theta_i)$$

$$\text{Eccentricity: } \epsilon = \sqrt{1 + \frac{2EL^2}{(GM)^2}}$$

$$R_0 = \frac{L^2}{GM}$$

$$\theta' = \theta_i + \cos^{-1}\left(\frac{R_0}{R_i} - \epsilon\right)$$

$$R_{\min} = R_0 / (1 + \epsilon)$$

$$\text{Semimajor Axis: } a = R_0 / (1 - \epsilon^2)$$

$$\text{Semiminor Axis: } b = a \sqrt{1 - \epsilon^2}$$

$$\text{Period: } T = 2\pi \sqrt{\frac{a^3}{GM}}$$

$$\text{Distance to Asymptote Vertex } S = R_{\min} (1 - \frac{1}{\epsilon})$$

$$\text{Angle between Asymptotes and } \theta_a = \cos^{-1}(\frac{1}{\epsilon})$$

Radius Vector

Given θ_{new} :

$$R_{\text{new}} = R_0 / (1 + \epsilon \cos(\theta_{\text{new}} - \theta'))$$

$$V_{\text{new}} = \sqrt{2(E + \frac{GM}{R_{\text{new}}})}$$

$$\alpha_{\text{new}} = \theta_{\text{new}} + \sin^{-1}\left(\frac{L}{V_{\text{new}} R_{\text{new}}}\right)$$

for a change in Velocity

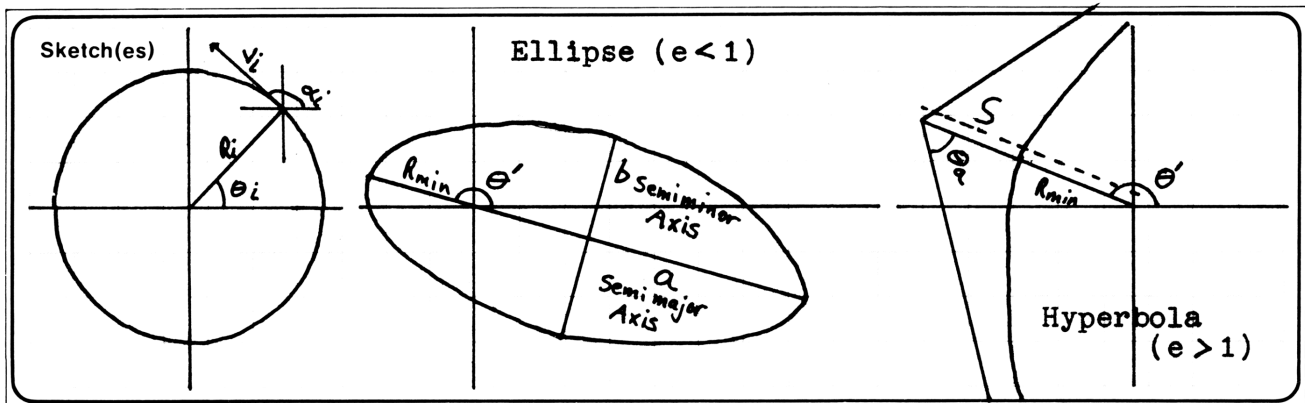
$$\vec{V}_{\text{new}} = \vec{V}_{\text{old}} + \Delta \vec{V}$$

Operating Limits and Warnings All angles should be $0 \leq \theta \leq 360$. If $\hat{\theta}$ (A) gives a negative radius for a hyperbolic orbit ($\epsilon > 1$) the orbit does not exist for the inputted θ . This program becomes ill-conditioned and inaccurate near degenerate conics (Circles, Parabolas and Straight lines). For added realism: avoid all orbits where $R_{\min} < \text{radius of the attracting body}$ (6.400×10^6 m for the Earth).

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II



Sample Problem(s) Execute a transfer from Low Earth Orbit to Geosynchronous

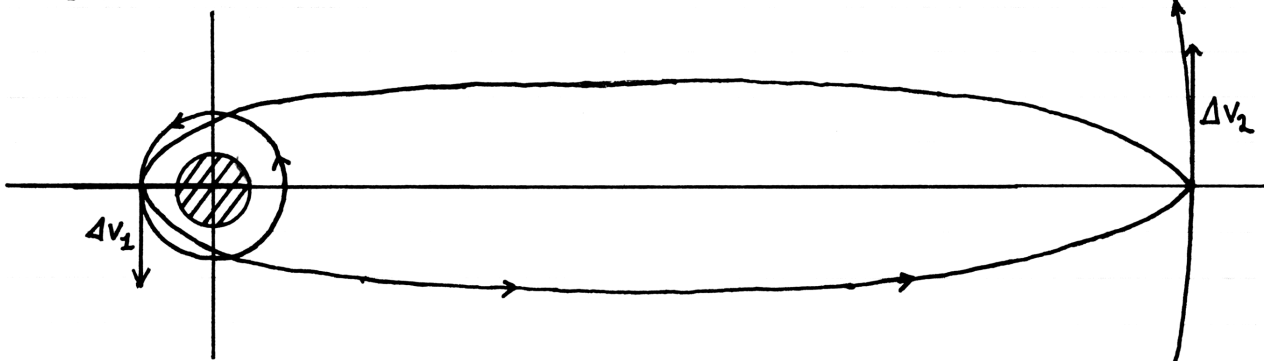
Step 1: Initialize $R_i = 7.1E6$ $\theta_i = 0$ $V_i = 7.4E3$ $\alpha_i = 90$

Step 2: Position Satellite at Perigee

Step 3: Accelerate to Synchronous Transfer

Step 4: Position Satellite at new Apogee

Step 5: Circularize



Solution(s) Keystrokes: (all underlined numbers are machine output)

Step 1: 7.10E6 ENT 0 F A

7.40E3 ENT 90 F B

Step 2: D 180.0 A 6.7462E6

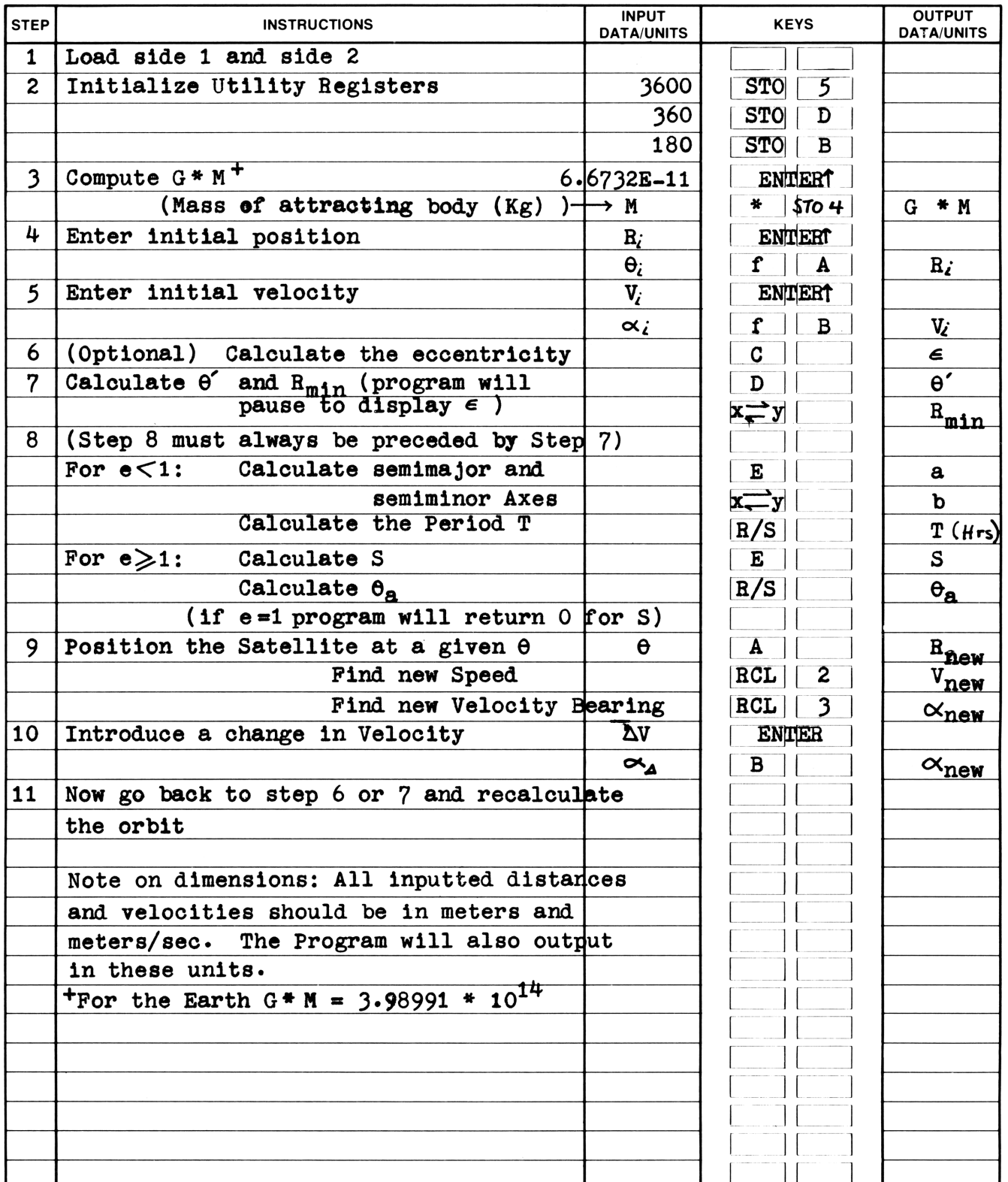
Step 3: 2312 RCL 3 B 270.0

Step 4: D 180.0 180 + A 4.228688E7

Step 5: 1455 RCL 3 B 90.0 C 3.505809E-3 E 4.213916E7
R/S 23.90148 H→H.MS 23.54053 *****

Reference(s) Goldstein: Classical Mechanics Chapt 3

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Note: All quantities listed below are per kilogram

Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	LBL a	32 25 11	67		RCL 8	34 08	
	STO 1	33 01			÷	81	
	$x \rightarrow y$	35 52			GSB d	32 22 14	
	STO 0	33 00		060	COS-1	32 63	
	RTN	35 22			RCL 3	34 03	
	LBL b	32 25 12			RCL 1	34 01	
	STO 3	33 03			-	51	
	$x \rightarrow y$	35 52			COS	31 63	
	STO 2	33 02			LST X	35 82	
010	SF 1	35 51 01			SIN	31 62	
	RTN	35 22			*	71	
	LBL C	31 25 13			$x < 0$	31 71	
	RCL 2	34 02			GTO 7	22 07	
	X**2	32 54		070	R↓	35 53	
	2	02			CHS	42	
	÷	81			R↑	35 54	
	RCL 4	34 04			LBL 7	31 25 07	
	RCL 0	34 00			R↓	35 53	
	÷	81			+	61	
020	-	51			GSB e	32 22 15	
	STO 6	33 06	→ ENERGY		STO A	33 11	→ θ'
	RCL 3	34 03			CLF 1	35 61 01	
	RCL 1	34 01			RCL 8	34 08	
	-	51		080	RTN	35 22	
	SIN	31 62			LBL D	31 25 14	
	RCL 0	34 00			TF 1	35 71 01	
	*	71			GSB C	31 22 13	
	RCL 2	34 02			RCL 8	34 08	
	*	71			Pause	35 72	
030	STO 7	33 07	→ ANGULAR MOMENTUM		1	01	
	X**2	32 54			+	61	
	2	02			1/X	35 62	
	*	71			RCL 9	34 09	
	RCL 6	34 06		090	*	71	→ R_{min}
	*	71			STO C	33 13	
	RCL 4	34 04			RCL A	34 11	
	X**2	32 54			RTN	35 22	
	÷	81			LBL E	31 25 15	
	1	01			TF 0	35 71 00	
040	+	61			GTO 2	22 02	
	$\sqrt{x}$	31 54			RCL 9	34 09	
	STO 8	33 08	→ ECCENTRICITY		1	01	
	1	01			RCL 8	34 08	
	CLF 0	35 61 00		100	X**2	32 54	
	$x \leq y$	32 71			-	51	
	STF 0	35 51 00			÷	81	
	RCL 1	34 01			STO E	33 15	→ Semimajor Axis
	RCL 7	34 07			LST X	35 82	
	X**2	32 54			$\sqrt{x}$	31 54	
050	RCL 4	34 04			*	71	→ Semiminor Axis
	÷	81			RCL E	34 15	
	STO 9	33 09	→ R_0		R/S	84	
	RCL 0	34 00			RCL E	34 15	
	÷	81		110	X**2	32 54	
	1	01			LST X	35 82	
	-	51			*	71	

REGISTERS

0 Dist	1 BEARING	2 Speed	3 Speed Bearing	4 G * M	5 3600	6 Energy	7 A. M.	8 e	9 R_0
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A θ'	B 180	C R_{min}	D 360	E a	I				

67 Program Listing II

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS											
	RCL 4	34 04			RCL 1	34 01												
	$\div$	81		170	RCL A	34 11												
	$\sqrt{x}$	31 54			-	51												
	2	02			SIN	31 62												
	*	71			*	71												
	π	35 73			x > 0	31 81												
	*	71			GTO 4	22 04												
120	RCL 5	34 05			CLX	44												
	$\div$	81		→Period (Hrs)	RCL B	34 12												
	RTN	35 22			-	51												
	LBL 2	31 25 02	Hyperbola Section	180	CHS	42												
	RCL C	34 13			R↑	35 54												
	1	01			LBL 4	31 25 04												
	RCL 8	34 08			R↓	35 53												
	1/X	35 62			RCL 1	34 01												
	-	51			+	61												
	x ≠ 0	31 61		Output Zero for a Parabola	GSB e	32 22 15		→α _{new}										
130	GTO 3	22 03				STO 3			33 03									
	RTN	35 22				RCL 0			34 00									
	LBL 3	31 25 03				RTN			35 22									
	$\div$	81			LBL B	31 25 12												
	R/S	84	→S		190	x $\Rightarrow$ y	35 52											
	RCL 8	34 08			→R	31 72												
	1/X	35 62			RCL 3	34 03												
	COS ⁻¹	32 63	→θ _a		RCL 2	34 02												
	RTN	35 22			→R	31 72												
	LBL A	31 25 11		x $\Rightarrow$ y	35 52													
140	STO 1	33 01			R↓		35 53											
	RCL A	34 11			+		61											
	-	51			R↓		35 53											
	COS	31 63			+		61											
	RCL 8	34 08			200		R↑	35 54										
	*	71			→P		32 72											
	1	01			STO 2		33 02											
	+	61			x $\Rightarrow$ y		35 52											
	RCL 9	34 09			GSB e		32 22 15											
	$\div$	81		STO 3	33 03													
150	1/X	35 62			SF 1		35 51 01											
	STO 0	33 00		→R _{new}	RTN		35 22											
	RCL 4	34 04			LBL e		32 25 15											
	x $\Rightarrow$ y	35 52			RCL D		34 14											
	$\div$	81			210		+	81										
	RCL 6	34 06			FRAC		32 83											
	+	61			1		01											
	2	02			+		61											
	*	71			FRAC		32 83											
	$\sqrt{x}$	31 54		RCL D	34 14													
160	STO 2	33 02			*		71											
	RCL 7	34 07		→V _{new}	RTN		35 22											
	RCL 0	34 00			LBL d		32 25 14											
	RCL 2	34 02			INT		31 83											
	*	71			220		x ≠ 0	31 61										
	$\div$	81			RTN		35 22											
	GSB d	32 22 14			CLX		44											
	SIN ⁻¹	32 62			LST X		35 82											
	RCL 7	34 07			RTN		35 22											
LABELS				FLAGS		SET STATUS												
A	θ	B	ΔV	C	∈	D	0, R _{min}	E	Graph	F	e ≥ 1	FLAGS		TRIG		DISP		
a	R ₁	b	V ₁	c		d	Adjust	e	Mod 360	1	Find e	ON OFF		DEG	☒	FIX	☐	
0		1		2	-used-	3	-used-	4	-used-	2		0	☐	☒	GRAD	☐	SCI	☒
5		6		7	-used-	8		9		3		1	☐	☒	RAD	☐	ENG	☐
												2	☐	☒			n	6
												3	☐	☒				

Program Description I

Program Title EQUATIONS OF PARTICLE MOTION

Contributor's Name ERIK GOETZE

Address 1613 CAMULOS AVE.

City GLENDALE

State CALIF

Zip Code 91208

Program Description, Equations, Variables HERE ALL VARIABLES ARE IN y , BUT ALL y 'S COULD BE REPLACED WITH x 'S.

nr1 $y = \frac{1}{2}(V_{y0} + V_y)t$

nr2 $y = V_{y0}t + \frac{1}{2}a_y t^2$ $V_{y0} = V_y - a_y t$ [nr10]

nr3 $y = \frac{V_y^2 - V_{y0}^2}{2a_y}$ $V_{y0} = \frac{2y}{t} - V_y$ [nr11]

nr4 $t = \frac{V_y - V_{y0}}{a_y}$ $V_{y0} = \frac{y}{t} - \frac{a_y t}{2}$ [nr12]

nr5 $t = \frac{2y}{V_{y0} + V_y}$ $V_{y0} = \sqrt{V_y^2 - 2a_y y}$ [nr13]

nr6 $t = (-V_{y0} \pm \sqrt{V_{y0}^2 + 2a_y y}) / a_y$

nr7 $V_y = V_{y0} + a_y t$ $a_y = \frac{V_y - V_{y0}}{t}$ [nr14]

nr8 $V_y = \frac{2y}{t} - V_{y0}$ [nr15] $a_y = 2 \left(\frac{y - V_{y0}t}{t^2} \right)$

nr9 $V_y = \sqrt{V_{y0}^2 + 2a_y y}$ [nr16] $a_y = \frac{V_y^2 - V_{y0}^2}{2y}$

y = DISTANCE COVERED BY PARTICLE IN TIME t

t = TIME IN WHICH PARTICLE MOVES

V_y = VELOCITY AT TIME t

V_{y0} = VELOCITY AT TIME 0

a_y = ACCELERATION (AVERAGE OVER TIME t) THAT PARTICLE IS EXPERIENCING IN TIME t

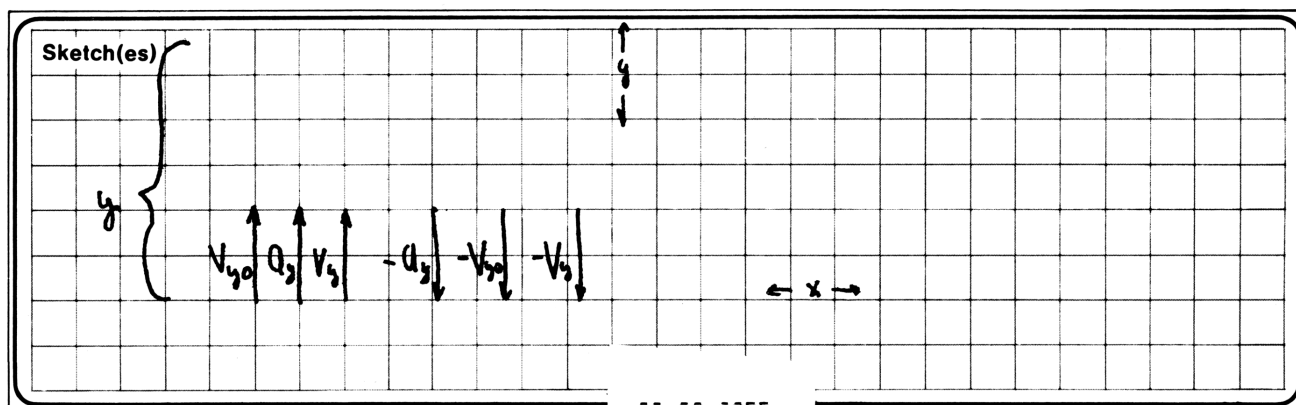
PROGRAM, GIVEN ANY THREE OUT OF THE ABOVE FIVE, WILL SOLVE THE ABOVE EQUATIONS FOR THE OTHER TWO.

Operating Limits and Warnings IF YOU ARE SOLVING FOR V -INITIAL, YOU MUST STORE THE VALUE YOU GET BY PRESSING [D] BEFORE SOLVING FOR THE OTHER UNKNOWN. THIS IS BECAUSE V_{y0} IS IN ALL THE OTHER EQUATIONS. IF THE DISPLAY COMES UP ERROR WHEN YOU ARE SOLVING FOR t , YOU HAVE AN IMAGINARY ROOT. SIMPLY SWITCH TO PROGRAM MORE, PRESS [SST] AND SWITCH BACK TO RUN AND PRESS [R/S]

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II



Sample Problem(s) **TEST**
EACH EQTN. GIVEN
ON PREVIOUS SHEET.

Clear everything **GSBe**

Initial vel. 256.00 **GSBD**

Final vel. 17.00 **GSBC**

Time (seconds) 8.60 **GSBB**

Solve for y 1.00 **GSBd**

1173.90 ***

GSBe

159.00 **GSBD**

4.80 **GSBB**

g down $\downarrow$ -9.80 **GSBE**

Solve for dist. 1.00 **GSBd**

650.30 ***

GSBe

12.00 **GSBC**

19.00 **GSBD**

-9.80 **GSBE**

1.00 **GSBd**

11.07 ***

Solve for time **GSBe**

29.00 **GSBD**

0.00 **GSBC**

-32.30 **GSBE**

2.00 **GSBd**

0.90 ***

0.00 **GSBe**

47.00 **GSBA**

28.00 **GSBD**

7.00 **GSBC**

2.00 **GSBd**

2.69 ***

GSBe

Quad roots
 pause $\rightarrow$

Solve for V_g

88.00 **GSBD**

-32.30 **GSBE**

12.00 **GSBA**

2.00 **GSBd**

5.31 ***

0.14 ***

GSBe

15.00 **GSBD**

-9.80 **GSBE**

2.50 **GSBB**

3.00 **GSBd**

-9.50 ***

GSBe

7.00 **GSBA**

1.80 **GSBB**

12.00 **GSBD**

3.00 **GSBd**

-4.22 ***

GSBe

-9.80 **GSBE**

5.00 **GSBA**

23.00 **GSBD**

3.00 **GSBd**

20.76 ***

GSBe

Solve for V_{y0}

19.00 **GSBC**

-9.80 **GSBE**

.38 **GSBB**

4.00 **GSBd**

22.72 ***

GSBe

14.80 **GSBA**

2.71 **GSBB**

0.00 **GSBC**

4.00 **GSBd**

10.92 ***

GSBe

Solve for a

118.00 **GSBA**

4.965 **GSBB**

-32.30 **GSBE**

4.00 **GSBd**

103.95 ***

GSBe

33.00 **GSBC**

-32.30 **GSBE**

15.70 **GSBA**

4.00 **GSBd**

45.86 ***

GSBe

24.70 **GSBC**

44.30 **GSBD**

2.00 **GSBB**

5.00 **GSBd**

-9.80 ***

GSBe

y down $\downarrow$

3.00 **GSBA**

18.00 **GSBD**

2.50 **GSBB**

5.00 **GSBd**

-13.44 ***

GSBe

17.00 **GSBC**

39.00 **GSBD**

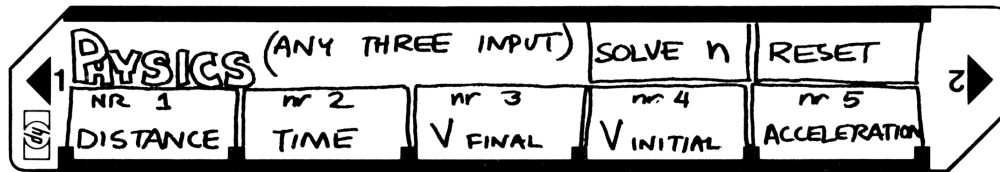
9.00 **GSBA**

5.00 **GSBd**

-68.44 ***

Reference(s) **PHYSICS BY RESNICK AND HALLIDAY CHAP 3 PAGE 49**

User Instructions

[illegible]

97 Program Listing I

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	*LBL9	21 09	
002	1	01		058	RCL0	36 00	
003	CF0	16 22 00	NR OF REG DIS IS STORED AT	059	RCL5	36 05	
004	GT00	22 00		060	=	-24	
005	*LBLB	21 12	NR OF REG TIME IS STORED AT	061	RTN	24	
006	2	02		062	*LBL2	21 02	
007	CF1	16 22 01		063	RCL5	36 05	
008	GT00	22 00		064	Pi	16-24	
009	*LBLC	21 13		065	X=Y?	16-33	
010	3	03	V FINAL NR REG	066	GT06	22 06	NO Acc
011	CF2	16 22 02		067	F0?	16 23 00	NO y
012	GT00	22 00		068	GT07	22 07	
013	*LBLD	21 14	V INITIAL NR REG	069	RCL4	36 04	
014	4	04		070	X²	53	
015	GT00	22 00		071	RCL5	36 05	
016	*LBLE	21 15	ACC. NR REG	072	RCL1	36 01	
017	5	05		073	2	02	
018	*LBL0	21 00		074	x	-35	
019	STOI	35 46		075	x	-35	
020	R↓	-31	STORE NR. IN REG	076	+	-55	
021	STOI	35 45		077	JX	54	
022	RCL3	36 03		078	ST09	35 09	
023	X²	53		079	RCL4	36 04	
024	RCL4	36 04	CALCULATE $\frac{V_y^2 - V_{y0}^2}{2}$	080	CHS	-22	
025	X²	53		081	+	-55	
026	-	-45		082	LSTX	16-63	
027	2	02		083	RCL9	36 09	
028	=	-24		084	-	-45	
029	ST00	35 00		085	RCL5	36 05	
030	CLX	-51		086	=	-24	
031	RTN	24		087	PSE	16 51	
032	*LBL1	21 01		088	LSTX	16-63	
033	F1?	16 23 01	DONT HAVE TIME	089	X*Y	-41	
034	GT09	22 09		090	R↓	-31	
035	F2?	16 23 02	DONT HAVE V FINAL	091	=	-24	
036	GT08	22 08		092	RTN	24	
037	RCL4	36 04		093	*LBL7	21 07	
038	RCL3	36 03		094	RCL3	36 03	
039	+	-55		095	RCL4	36 04	
040	RCL2	36 02	CALCULATE y USING FORMULA NR 1	096	-	-45	
041	x	-35		097	RCL5	36 05	
042	2	02		098	=	-24	
043	=	-24		099	RTN	24	
044	RTN	24		100	*LBL6	21 06	
045	*LBL8	21 08		101	RCL1	36 01	
046	RCL4	36 04		102	2	02	
047	RCL2	36 02		103	x	-35	
048	x	-35		104	RCL3	36 03	
049	RCL2	36 02	CALCULATE y USING FORMULA NR 2	105	RCL4	36 04	
050	X²	53		106	+	-55	
051	RCL5	36 05		107	=	-24	
052	x	-35		108	RTN	24	
053	2	02		109	*LBL3	21 03	
054	=	-24		110	F0?	16 23 00	
055	+	-55		111	GT09	22 09	
056	RTN	24		112	F1?	16 23 01	

CALCULATE y
USING FORMULA
NR 3

NO Acc
NO y

QUAD ROOT
EVALUATION
FOR t
USING FORMULA
NR 6

CALCULATE T
USING FORMULA
NR 4

CALCULATE T
USING FORMULA
NR 5

NO y

REGISTERS

0 $V_y^2 - V_{y0}^2$	1 DIST.	2 TIME	3 V_{FINAL}	4 $V_{INITIAL}$	5 ACCELER.	6	7	8	9 $\sqrt{b^2 - 4ac}$
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C	D	E	NR OF LABEL + REG				

97 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS	
113	GT0a	22 16 11	CALCULATE V_f USING FORMULA NR 8	169	RCL5	36 05	CALCULATE V_{y0} USING FORMULA NR 13	
114	RCL1	36 01		170	RCL1	36 01		
115	2	02		171	2	02		
116	x	-35		172	x	-35		
117	RCL2	36 02		173	x	-35		
118	$\div$	-24	CALCULATE V_f USING FORMULA NR 7	174	-	-45	CALCULATE V_{y0} USING FORMULA NR 11	
119	RCL4	36 04		175	JX	54		
120	-	-45		176	RTN	24		
121	RTN	24		177	*LBL8	21 08		
122	*LBL9	21 09		178	RCL1	36 01		
123	RCL4	36 04	CALCULATE V_f USING FORMULA NR 9	179	2	02	CALCULATE Q USING FORMULA NR 15	
124	RCL5	36 05		180	x	-35		
125	RCL2	36 02		181	RCL2	36 02		
126	x	-35		182	$\div$	-24		
127	+	-55		183	RCL3	36 03		
128	RTN	24	CALCULATE V_{y0} USING FORMULA NR 12	184	-	-45	CALCULATE Q USING FORMULA NR 14	
129	*LBLa	21 16 11		185	RTN	24		
130	RCL4	36 04		186	*LBL5	21 05		
131	X ²	53		187	F0?	16 23 00		
132	RCL1	36 01		188	GT07	22 07		
133	RCL5	36 05	CALCULATE V_{y0} USING FORMULA NR 10	189	F1?	16 23 01	CALCULATE Q USING FORMULA NR 16	
134	2	02		190	GT06	22 06		
135	x	-35		191	RCL1	36 01		
136	x	-35		192	RCL4	36 04		
137	+	-55		193	RCL2	36 02		
138	JX	54	CALCULATE V_{y0} USING FORMULA NR 10	194	x	-35	RESET BY SETTING FLAGS, π IN R ₅	
139	RTN	24		195	-	-45		
140	*LBL4	21 04		196	RCL2	36 02		
141	F0?	16 23 00		197	X ²	53		
142	GT0b	22 16 12		198	$\div$	-24		
143	F1?	16 23 01	CALCULATE V_{y0} USING FORMULA NR 10	199	2	02	CALCULATE VARIABLE i IN ROUTINE i	
144	GT0c	22 16 13		200	x	-35		
145	RCL5	36 05		201	RTN	24		
146	Pi	16-24		202	*LBL7	21 07		
147	X=Y?	16-33		203	RCL3	36 03		
148	GT08	22 08	CALCULATE V_{y0} USING FORMULA NR 10	204	RCL4	36 04	CALCULATE VARIABLE i IN ROUTINE i	
149	RCL1	36 01		205	-	-45		
150	RCL2	36 02		206	RCL2	36 02		
151	$\div$	-24		207	$\div$	-24		
152	RCL5	36 05		208	RTN	24		
153	RCL2	36 02	CALCULATE V_{y0} USING FORMULA NR 10	209	*LBL6	21 06	CALCULATE VARIABLE i IN ROUTINE i	
154	x	-35		210	RCL0	36 00		
155	2	02		211	RCL1	36 01		
156	$\div$	-24		212	$\div$	-24		
157	-	-45		213	RTN	24		
158	RTN	24	CALCULATE V_{y0} USING FORMULA NR 10	214	*LBLc	21 16 15	CALCULATE VARIABLE i IN ROUTINE i	
159	*LBLb	21 16 12		215	SF0	16 21 00		
160	RCL3	36 03		216	SF1	16 21 01		
161	RCL5	36 05		217	SF2	16 21 02		
162	RCL2	36 02		218	Pi	16-24		
163	x	-35	CALCULATE V_{y0} USING FORMULA NR 10	219	ST05	35 05	CALCULATE VARIABLE i IN ROUTINE i	
164	-	-45		220	0	-00		
165	RTN	24		221	RTN	24		
166	*LBLc	21 16 13		222	*LBLd	21 16 14		
167	RCL3	36 03		223	ST01	35 46		
168	X ²	53	LABELS	224	GT0i	22 45	SET STATUS	
A STORE DIS	B STORE TIME	C STORE V_f	D STORE V_{in}	E STORE A_{in}	0 SET IF DIS HASN'T ENTERED	FLAGS	TRIG	DISP
a USED	b USED	c USED	d SOLVE	e RESET	1 SET IF TIME HASN'T ENTERED	ON OFF	DEG ☒	FIX ☒
0 STORAGE	1 CALC DIS	2 CALC TIME	3 CALC V_f	4 CALL V_{init}	2 SET IF V_f HASN'T ENTERED	0 ☒	GRAD ☐	SCI ☐
5 CALL A_{in}	6 USED	7 USED	8 USED	9 USED	3	1 ☒	RAD ☐	ENG ☐
						2 ☐		n 2
						3 ☐		

Program Description I

Program Title	Ballistics Trajectory Computations		
Contributor's Name	David M. Ivey		
Address	2470 New Clinton Rd.		
City	Macon	State	Ga. Zip Code 31201

Program Description, Equations, Variables The Program computes remaining velocities, energies, flight times, maximum rise and drops of bullets at user specified intervals. Computations technically apply to ICAO conditions which are satisfactory for most shooting conditions. The method uses a Mayevski drag formulation ($\text{drag} = Av^n$) with different constants for different velocity zones. The program automatically selects the correct constants. Program control is by Label A, the various data outputs are done by Labels 2,3,4,5, and 6 so that users may easily arrange output data order. Label 7 computes air resistance. Note that maximum rise gives sight in data.

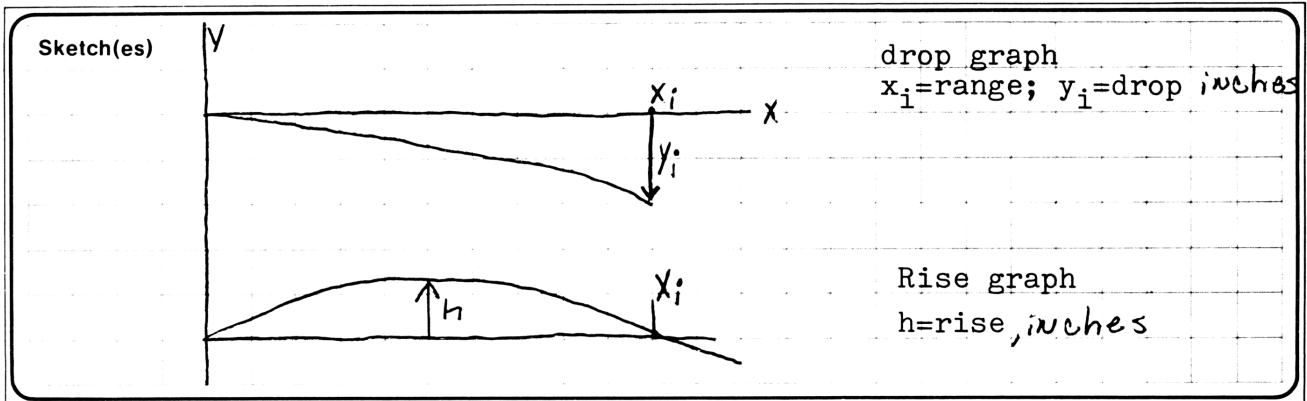
Use English Units Only

Operating Limits and Warnings Be sure to use ballistic coefficients based on Ingall's Tables (most are, usual exceptions are foreign bullets). This system works best when the coefficient (C_b) is greater than .150 and velocities above that of sound. Most importantly however, use range intervals no greater than 100yds, shorter intervals give better accuracy. For typical rifles about 3% error occurs relative to numeric integration techniques at 1000yards.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II



Sample Problem(s) Compute the complete trajectory of a 30/06 cartridge where the bullet weight is 165grain Sierra boat-tail (ballistic coefficient for this bullet=0.470) at a muzzle velocity of 2800ft/sec in 100yd. intervals out to 200yards.

Velocity in ft/sec
 Energy in ft lbs
 time in seconds
 Rise & drop in inches

Muzzle Vel $\rightarrow$ 2800. ***
 Bullet wt $\rightarrow$ 165. ***
 $C_B \rightarrow$ 0.470 ***

Solution(s) Input keystrokes

$C_B=0.470$ STO 6

$\Delta x=300$ feet STO 7

$x_m=200$ yds=600ft use 601 to stop.

601 STO 8

$w_b=165$ STO 9

$V_o=2800$ STO A

Set flags Zero and One to

output energy and rise Press A

Range yds 100. ***

Velocity 2585. ***

Energy 2454. ***

time 0.1114 sec ***

Rise 0.66" ***

drop 2.33" ***

200. ***

2385. ***

2684. ***

0.2328 ***

2.58 ***

9.86 ***

Output $\Rightarrow$

Reference(s) This program represents the first complete ballistic system without extensive numeric integration techniques or long tables. It was specifically developed for microcomputer applications. For more information regarding theoretical development, write the author.

DAVID M. IVEY

2470 NEW CLINTON RD.

MACON, GEORGIA 31201

PH (912) 743-4206

Ballistics Trajectory Computations

A) Equations;

$$V_f = [V_i^2 - Z'D]^{1/2}$$

$$D = AV_i^N$$

$$Z' = \frac{2\Delta X}{c}$$

$$t_f = 2\Delta X \sum_{i=1}^N \frac{1}{V_i + V_f}$$

$$h = 48.26 t_f^2$$

$$Y_f = \frac{4}{3} h (1 + 2\sqrt{V_f/V_0})$$

$$E_f = \frac{W_8 V_f^2}{450240}$$

(W₈ in grains)

B) Note the constants A and N are stored in registers by the data card.

Mayevski Velocity Zones

Range of V	N	A
3600 to 2600	1.55	4.064882535(10 ⁻³)
2600 to 1800	1.70	1.247951766(10 ⁻³)
1800 to 1370	2.00	1.316(10 ⁻³)
1370 to 1230	3.00	9.569787630(10 ⁻⁸)
1230 to 970	5.00	6.336817507(10 ⁻¹⁴)

Location of Constants

The N, A values occupy secondary storage registers. Zone Velocities occupy Registers B to E

Below is a print out of Register Contents:

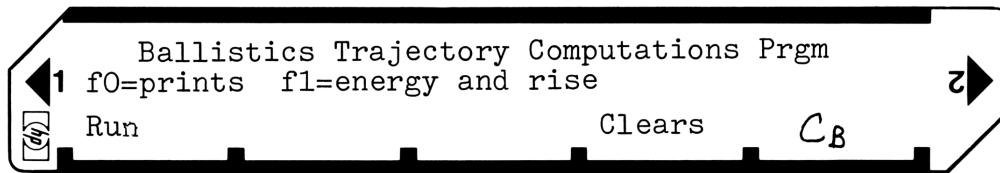
```

4.064882535-03 10
1.55 11
1.247951766-03 12
1.7 13
1.316000000-03 14
2.0 15
9.569787630-03 16
3.0 17
6.336817507-14 18
5.0 19
0.0 A
1800.0 B
1370.0 C
1230.0 D
970.0 E
0.0 I

```

10 Refers to
Address of
storage
Register

User Instructions



STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
1	Load Program Card, Both sides			
	Load Data Card, Both sides			
2	Store Parameters Ballistic coefficient	C_b	STO 6	C_b
	Range Increment (ft)	Δx	STO 7	Δx
	Maximum Range ft	X_m	STO 8	X_m
	Bullet weight Grains	w_b	STO 9	w_b
	Muzzle Velocity	V_o	STO A	V_o
3	Set Output status			
	Flag Zero set will Print ans, else pause			
	Flag One set will compute Energy and rise according to Flag Zero's status			
4	Execute program Press LBL A			
	Prgm first outputs initial data			V_o
				w_b
				C_b
	Then the computations :			
				Range
				Velocity
				energy
				time
				rise
				drop
5	New Problem go to Step two after clearing by LBL C			
6	To Compute a ballistic Coefficient by Ingalls			
	A STORE Range between	ΔX	STO 7	ΔX
	Known velocities			
	Enter Velocities	V_i	$\uparrow$	V_i
		V_{i+1}	$\downarrow$	$-C_B$

97 Program Listing I

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11	Prgrm Control Initial Settings	057	CHS	-22	Energy Calculations
002	F0?	16 23 00		058	RCL4	36 04	
003	SFC	16-11		059	X ²	53	
004	GSB0	23 14		060	+	-55	
005	RCL7	36 07		061	JX	54	
006	ST02	35 02		062	GSB1	23 01	
007	1	01		063	RTN	24	
008	0	00		064	*LBL3	21 03	
009	ST01	35 46		065	RCL4	36 04	
010	RCLA	36 11		066	X ² Y	-41	
011	ST04	35 04	Initial Data Output	067	+	-55	Flight Time Calculations
012	GSB1	23 01		068	LSTX	16-63	
013	RCL9	36 09		069	ST04	35 04	
014	GSB1	23 01		070	X ² Y	-41	
015	RCL6	36 06		071	ST03	35 03	
016	DSP3	-63 03		072	RCL4	36 04	
017	GSB1	23 01		073	X ²	53	
018	DSP0	-63 00		074	RCL9	36 09	
019	F0?	16 23 00		075	x	-35	
020	SFC	16-11		076	4	04	
021	*LBLB	21 12	Main Prgrm Control after initialization	077	5	05	Rise (Maximum Ordinate) calculations
022	F0?	16 23 00		078	0	00	
023	SFC	16-11		079	2	02	
024	GSB8	23 08		080	4	04	
025	F0?	16 23 00		081	0	00	
026	SFC	16-11		082	÷	-24	
027	GSB2	23 02		083	F1?	16 23 01	
028	GSB3	23 03		084	GSB1	23 01	
029	GSB4	23 04		085	RTN	24	
030	GSB5	23 05		086	*LBL4	21 04	
031	GSB6	23 06	} data Computations	087	RCL3	36 03	Velocity Computations
032	RCL7	36 07		088	1/X	52	
033	ST+2	35-55 02		089	2	02	
034	RCL2	36 02		090	x	-35	
035	RCL8	36 08		091	RCL7	36 07	
036	X ² Y?	16-35		092	x	-35	
037	RTN	24		093	ST+5	35-55 05	
038	GTOB	22 12		094	x	-35	
039	*LBL1	21 01		095	RCL5	36 05	
040	F0?	16 23 00		096	DSP4	-63 04	
041	GTOa	22 16 11	Pause or Print Routine	097	F1?	16 23 01	Rise (Maximum Ordinate) calculations
042	PSE	16 51		098	GSB1	23 01	
043	PSE	16 51		099	RTN	24	
044	RTN	24		100	*LBL5	21 05	
045	*LBLa	21 16 11		101	X ²	53	
046	PRTX	-14		102	4	04	
047	RTN	24		103	6	06	
048	*LBL2	21 02		104	.	-62	
049	RCL4	36 04		105	2	02	
050	GSB7	23 07		106	6	06	
051	RCL7	36 07	Velocity Computations	107	x	-35	Rise (Maximum Ordinate) calculations
052	x	-35		108	DSP2	-63 02	
053	2	02		109	GSB1	23 01	
054	x	-35		110	RTN	24	
055	RCL6	36 06		111	*LBL6	21 06	
056	÷	-24		112	4	04	

REGISTERS

0	1	2	3	4	5	6	7	8	9
		X_i	used	V_i	$\sum \frac{1}{v_i + v_k}$	C_B	ΔX	X_m	W_B
S0 4.064(10 ⁻³)	S1 1.55	S2 1.24(10 ⁻³)	S3 1.70	S4 1.31(10 ⁻³)	S5 2.00	S6 9.57(10 ⁻³)	S7 3.00	S8 6.34(10 ⁻⁴)	S9 5.00
A V_0	B 1800	C 1370	D 1230	E 970	I USED UNRECORDED				

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	X	-35	LBL 6 drop Computation	169	GTOb	22 16 12	Clears time Register and Range counter Outputs range in yards
114	3	03		170	*LBL e	21 16 15	
115	=	-24		171	1	01	
116	RCL4	36 04		172	4	04	
117	RCL A	36 11		173	STOI	35 46	
118	=	-24		174	GTOb	22 16 12	
119	JX	54		175	*LBL d	21 16 14	
120	2	02		176	1	01	
121	x	-35		177	0	00	
122	1	01		178	STOI	35 46	
123	+	-55	179	GTOb	22 16 12	Ballistic Coefficient Calculations	
124	x	-35	180	*LBL d	21 14		
125	GSB1	23 01	181	0	00		
126	RTN	24	182	STO2	35 02		
127	*LBL7	21 07	183	STO5	35 05		
128	2	02	184	RTN	24		
129	6	06	185	*LBL8	21 06		
130	EEX	-23	186	RCL2	36 02		
131	2	02	187	3	03		
132	XZY?	16-35	188	=	-24		
133	GTOb	22 00	189	DSP0	-63 00		
134	XZY	-41	190	GSB1	23 01		
135	RCLB	36 12	191	RTN	24		
136	XZY?	16-35	192	*LBL e	21 15		
137	GTOb	22 16 13	193	STO0	35 00		
138	XZY	-41	194	XZY	-41		
139	RCLC	36 13	195	STOI	35 01		
140	XZY?	16-35	196	STO4	35 04		
141	GTOb	22 16 15	197	GSB7	23 07		
142	XZY	-41	198	2	02		
143	RCLD	36 14	199	x	-35		
144	XZY?	16-35	200	RCL7	36 07		
145	GTOb	22 16 14	201	x	-35		
146	1	01	202	RCL1	36 01		
147	0	00	203	X ²	53		
148	STOI	35 46	204	CHS	-22		
149	*LBL b	21 16 12	205	RCL0	36 00		
150	RCL4	36 04	206	X ²	53		
151	RCL i	36 45	207	+	-55		
152	ISZI	16 26 46	208	=	-24		
153	RCL i	36 45	209	GSB1	23 01		
154	XZY	-41	210	RTN	24		
155	R4	-31	211	R/S	51		
156	YX	31					
157	R1	16-31					
158	x	-35					
159	RTN	24					
160	*LBL0	21 00	Labels 0, C, e d assure correct constant for drag velocity Zone				
161	1	01					
162	0	00					
163	STOI	35 46					
164	GTOb	22 16 12					
165	*LBL c	21 16 13					
166	1	01					
167	2	02					
168	STOI	35 46					
LABELS				FLAGS		SET STATUS	
A Initial Cont	B used	C	D Clears	E $V_{i+1} \rightarrow C_B$	0 Prints	FLAGS	
^a used	^b used	^c Zones	^d Zones	^e Zones	¹ Does Ft rise	TRIG	
⁰ Zones	¹ Print/Pause	² Velocity	³ Energy	⁴ time	²	DISP	
⁵ rise	⁶ drop	⁷ drag	⁸ Range	⁹	³		
						ON OFF	
						0 ☒ ☐	DEG ☒
						1 ☐ ☐	GRAD ☐
						2 ☐ ☒	RAD ☐
						3 ☐ ☒	FIX ☒
							SCI ☐
							ENG ☐
							n 2,4,0

Program Description I

Program Title ISOTOPE OVERLAP CORRECTIONS

Contributor's Name Lawrence I. Grossman

Address 206 Crest Ave.

City Ann Arbor

State MI

Zip Code 48103

Program Description, Equations, Variables Program Corrects for spillover between channels when two radioactive isotopes are being counted in a liquid scintillation spectrometer. Background subtraction for each isotope is also provided. Program may be used with single isotope.

Isotopes x and y are counted in machine channels A and B, respectively.

Let a = fractional spillover of isotope y from channel B to A.

b = fractional spillover of isotope x from channel A to B.

C_x = corrected counts/min isotope x in channel A = $\frac{C_A - a C_B}{1 - ab}$, where C_A and C_B are the observed counts/min in each channel.

$$C_y = \frac{C_B - b C_A}{1 - ab}$$

Outputs

Total counts/min isotope x = $C_x (1 + b) = T_x$

Total counts/min isotope y = $C_y (1 + a) = T_y$

Operating Limits and Warnings

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Program Description II

Sketch(es)

Sample Problem(s) 2 isotopes. Spillover $A \rightarrow B = 10\%$, $B \rightarrow A = 20\%$, $Bk_A = 10$ cpm, $Bk_B = 50$ cpm

For the following values of cts/min_A and cts/min_B , calculate corrected values and totals.

sample [#]	A	B
1	1000	500
2	2000	1000
3	1400	2200

Solution(s) Keystrokes

[F] [A] $\rightarrow 0.00$
 0.2 ENTER 10 [D] $\rightarrow 0.20$
 0.1 ENTER 50 [E] $\rightarrow 0.10$
 1 [F] [C] $\rightarrow 1.00$
 1000 [A] 500 [B] [C] $\rightarrow 1010$ (T_x)
 $\rightarrow 430$ (T_y)
 $\rightarrow 2$ (next sample)
 2000 [A] 1000 [B] [C] $\rightarrow 2020$ (T_x)

$\rightarrow 920$ (T_y)
 $\rightarrow 3$ (next)
 1400 [A] 2200 [B] [C] $\rightarrow 1078$ (T_x)
 $\rightarrow 2462$ (T_y)
 $\rightarrow 4$ (next)
 [F] [B] $\rightarrow 4108$ (ΣT_x)
 $\rightarrow 3812$ (ΣT_y)
 $\rightarrow 0$ (reset)

Reference(s)

45

ISOTOPE OVERLAP CORRECTIONS

1

2 LABELS? $\rightarrow \epsilon_{Tx}, \epsilon_{Ty}$ 1st free. No.

CPM-A CPM-B $\rightarrow T_x, T_y$ $B \rightarrow A \uparrow B k_a$ $A \rightarrow B \uparrow B k_b$

2

[illegible]

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBL D	31 25 14			X	71	
	STO 0	33 00	store BKA, a		STO +8	33 61 08	
	R+	35 53			STO 9	33 09	
	STO 1	33 01		060	RCL 7	34 07	output Tx,
	RTN	35 22			-X-	31 84	Ty (if Fo set)
	*LBL C	32 25 13	store first sample no.		RCL 9	34 09	
	ST I	35 33			FO?	35 71 00	
	RTN	35 22			-X-	31 84	
	*LBL E	31 25 15			ISZ	31 34	
010	STO 2	33 02	store BKB, b		RCL I	35 34	
	R+	35 53			RTN	35 22	
	STO 3	33 03			*LBL a	32 25 11	SFO for 2 labels
	RTN	35 22			SFO	35 51 00	
	*LBL A	31 25 11	enter counts/min for A	070	RTN	35 22	
	RCL 0	34 00	channel, subtract BKA,		*LBL b	32 25 12	output total x for
	-	51	store.		RCL 6	34 06	all samples, total y
	STO 4	33 04			-X-	31 84	(if Fo set). CFO.
	RTN	35 22			RCL 8	34 08	Clear accumulation
	*LBL B	31 25 12	enter counts/min for B		FO?	35 71 00	registers.
020	RCL 2	34 02	channel, subtract BKB,		-X-	31 84	
	-	51	store		CFO	35 61 00	
	STO 5	33 05			0	00	
	RTN	35 22		080	STO 6	33 06	
	*LBL C	31 25 13	Calculate Cx, Cy,		STO 8	33 08	
	RCL 4	34 04	Tx, Ty		ST I	35 33	
	RCL 1	34 01			RTN	35 22	
	RCL 5	34 05					
	X	71					
	-	51					
030	1	01					
	RCL 1	34 01					
	RCL 3	34 03					
	X	71					
	-	51					
	÷	81					
	1	01					
	RCL 3	34 03					
	+	61					
	X	71					
040	STO +6	33 61 06					
	STO 7	33 07					
	DISP 0	23 00					
	RCL 5	34 05					
	RCL 3	34 03					
	RCL 4	34 04					
	X	71					
	-	51					
	1	01					
	RCL 1	34 01					
050	RCL 3	34 03					
	X	71					
	-	51					
	÷	81					
	1	01					
	RCL 1	34 01					
	+	61					

LABELS				
A	B	C	D	E
counts/min A	counts/min B	output Tx, Ty	a ↑ Background A	b ↑ Background B
a	b	c	d	e
2 labels	Total cpm	1 st sample No.		
0	1	2	3	4
5	6	7	8	9

FLAGS		SET STATUS		
0 Set for 2 isotopes		FLAGS	TRIG	DISP
1		ON OFF		
		0 ☒ ☐	DEG ☒	FIX ☒
2		1 ☐ ☒	GRAD ☐	SCI ☐
		2 ☐ ☒	RAD ☐	ENG ☐
110		3 ☐ ☒		n 0

REGISTERS									
0	1	2	3	4	5	6	7	8	9
Background A	a	Background B	b	CA	CB	ΣCx	Cx	ΣCy	Cy
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C	D	E	I	sample Number			

Program Description I

Program Title Critical Reactor Code

Contributor's Name Richard D. Hyman

Address 23822 80th W.

City Edmonds

State Washington

Zip Code 98020

Program Description, Equations, Variables The program estimates the parameters of a reactor with different fuels, moderator, fuel to moderator ratios, size, and shapes of the reactor. Its most important use is in indicating trends in certain changes of mod. etc.

$$\eta = \frac{\gamma_{235}\Sigma_f(235)}{\Sigma_a(235)+\Sigma_a(238)} = \gamma \frac{\sigma_f}{\sigma_a}$$

$$f = \frac{\Sigma_a F}{\Sigma_a t} = \frac{\Sigma_a m}{\Sigma_a F} \frac{V_m}{V_F} F + E$$

$$F(x) = 1 + \frac{1}{2} \left(\frac{x}{2}\right)^2 - \frac{1}{12} \left(\frac{x}{2}\right)^4 + \frac{1}{48} \left(\frac{x}{2}\right)^6 : x = a/LF$$

$$E(y,z) = 1 + \frac{z^2}{2} \left[\frac{z^2}{z^2 - y^2} \ln\left(\frac{z}{y}\right) - \frac{3}{4} + \frac{y^2}{4z^2} \right] : \begin{matrix} z = b/LM \\ y = a/LM \end{matrix}$$

$$\rho = \exp - \left[\frac{N_F V_F I}{\Sigma_m \Sigma_{sm} V_m} \right] \quad I = A + C / \sqrt{a\rho}$$

$$B^2 = \left(\frac{\pi}{R}\right)^2 \text{ sphere}$$

$$\epsilon = 1 + .3 \left(\frac{V_F}{V_m}\right)$$

$$P_L = \frac{1}{1 + B^2 L_T}$$

$$B^2 = 3\left(\frac{\pi}{R}\right)^2 \text{ cube}$$

Operating Limits and Warnings This program works best for low enrichment fuel, (-7²-5)% this is much like a power reactor. The accuracy is only to be taken as an estimate. But the trends are good. Note: Radius of reactor is stored in S-6 register to change this you must change [P↔S] [STO 6] [P↔S]

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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New data cards can be made for U^{235} Pu^{239} fuels & H_2O , C, on D_2O moderators. The information needed on these cards can be found in John R. Lamarsh, Introduction to Nuclear Engineering.

P-0 = ρ - Density of Fuel

P-1 = MW - Molecular weight of fuel

P-2 = Atom density of fuel

P-3 = $\Sigma_a F$ - Microscopic cross section of fuel (abs.)(cm⁻¹)

P-4 = Microscopic cross section of mod. (abs.) (cm⁻¹)

P-5 = Const A

P-6 = Const C

P-7 = $\Sigma_m \Sigma_{sm}$

P-8 = Microscopic fission cross section of fuel (in barns)

P-9 = # of neutrons emitted per fission

S-8 = Diffusion length of moderator (cm)

S-9 = Diffusion length of fuel (cm)

A = Enrichment % of fissile fuel

B = Microscopic abs - cross section of fissile fuel (in barns)

C = Microscopic abs cross section of U^{238} (in barns)

D = Radius of fuel pin (cm)

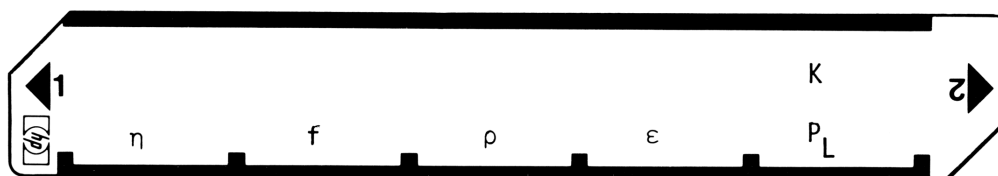
E = Radius of fuel

All these must be set for different fuel + moderators this is why it is best to record this on a card.

Values for Diff. Fuel + Moderators

	U^{235}	Pu^{239}	H_2O	D_2O	C
ρ	19.1	21.45			
MW	238	239			
NF	.04833	.04938			
ΣaF					
Σam			.0222	2.9×10^{-5}	.0002728
A	3.0	3.0			
C	38	38			
$\Sigma m \Sigma sm$			1.46	.178	.0608
σf	580	742.5			
γ	2.6	2.98			
Lm			2.85	170	59
L_F	1.55	2.0			
$\sigma a f_{iss}$	680	1011.3			
σa_{238}	2.7	2.7			

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[illegible]

Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS			
001	*LBLA	21 11	Calculates η	057	6	06				
002	1	01		058	Y*	31				
003	0	00		059	4	04				
004	0	00		060	8	08				
005	RCLA	36 11		061	1/X	52				
006	-	-45		062	x	-35				
007	RCLA	36 11		063	RCLI	36 46				
008	$\div$	-24		064	4	04				
009	RCLC	36 13		065	Y*	31				
010	x	-35		066	1	01				
011	RCLB	36 12		067	2	02				
012	+	-55		068	1/X	52				
013	RCL8	36 08		069	x	-35				
014	RCL9	36 09		070	CHS	-22				
015	x	-35		071	+	-55				
016	X*Y	-41	072	RCLI	36 46					
017	$\div$	-24	073	X ²	53					
018	P*S	16-51	074	.	-62					
019	ST00	35 00	075	5	05					
020	ST05	35 05	076	x	-35					
021	P*S	16-51	077	+	-55					
022	RTN	24	078	1	01					
023	*LBLB	21 12	079	+	-55					
024	RCL0	36 00	080	RCLC	36 15					
025	RCL1	36 01	081	X ²	53					
026	$\div$	-24	082	ST01	35 46					
027	.	-62	083	RCLD	36 14					
028	6	06	084	X ²	53					
029	0	00	085	-	-45					
030	2	02	086	RCLI	36 46					
031	3	03	087	$\div$	-24					
032	x	-35	088	x	-35					
033	ST02	35 02	089	P*S	16-51					
034	RCLA	36 11	090	RCL4	36 04					
035	%	55	091	RCL3	36 03					
036	RCLB	36 12	092	$\div$	-24					
037	x	-35	093	x	-35					
038	1	01	094	P*S	16-51					
039	0	00	095	ST01	35 01					
040	0	00	096	RCLC	36 15					
041	RCLA	36 11	097	RCL8	36 08					
042	-	-45	098	$\div$	-24					
043	RCL2	36 02	099	ST01	35 46					
044	X*Y	-41	100	RCLD	36 14					
045	%	55	101	RCL8	36 08					
046	RCLC	36 13	102	$\div$	-24					
047	x	-35	103	$\div$	-24					
048	+	-55	104	LN	32					
049	ST03	35 03	105	RCLI	36 46					
050	P*S	16-51	106	X ²	53					
051	RCLD	36 14	107	RCLD	36 14					
052	RCL9	36 09	108	RCL8	36 08					
053	$\div$	-24	109	$\div$	-24					
054	2	02	110	X ²	53					
055	$\div$	-24	111	-	-45					
056	ST01	35 46	112	RCLI	36 46					
REGIS										
0	ρ	1 MW fuel	2 N fuel	3 ΣaF	4 Σam	5 A	6 C	7 $\Sigma sm \Sigma sm$	8 σf_{25}	9 γ
S0 η	S1 f	S2 ρ	S3 ϵ	S4 P_L	S5 K	S6 Radius (cm)	S7	S8 L_M	S9 L_F	
A enrich %		B σ_a fiss. fuel		C σ_a non fiss fuel		D a (cm)		E b (cm)		I used

Program Listing II

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	X ²	53		169	e ^x	33	
114	X ² Y	-41		170	P ² S	16-51	
115	÷	-24		171	STO2	35 02	
116	x	-35		172	STx5	35-35 05	
117	.	-62		173	P ² S	16-51	End of ρ
118	7	07		174	RTN	24	
119	5	05		175	*LBLD	21 14	
120	-	-45		176	RCLD	36 14	
121	RCLD	36 14		177	X ²	53	
122	RCL8	36 08		178	STOI	35 46	
123	÷	-24		179	RCLF	36 15	
124	4	04		180	X ²	53	Calculates
125	÷	-24		181	RCLI	36 46	ε
126	RCLI	36 46		182	-	-45	
127	÷	-24		183	÷	-24	
128	RCLI	36 46		184	.	-62	
129	÷	-24		185	1	01	
130	+	-55		186	x	-35	
131	RCLI	36 46		187	1	01	
132	X ²	53		188	+	-55	
133	x	-35		189	P ² S	16-51	
134	2	02		190	STO3	35 03	
135	÷	-24		191	STx5	35-35 05	
136	1	01		192	P ² S	16-51	
137	+	-55		193	RTN	24	
138	RCL1	36 01		194	*LBLF	21 15	
139	+	-55		195	P ² S	16-51	
140	1/X	52		196	Pi	16-24	Calculates
141	STOI	35 01	End of f	197	RCL6	36 06	
142	STx5	35-35 05		198	÷	-24	P _L
143	P ² S	16-51		199	X ²	53	
144	RTN	24		200	F1?	16 23 01	
145	*LBLC	21 13		201	STOI	22 01	
146	RCL0	36 00		202	3	03	
147	RCLD	36 14		203	x	-35	
148	x	-35		204	*LBL1	21 01	
149	√X	54		205	STOI	35 46	
150	RCL6	36 06	Calculates	206	RCL8	36 08	
151	X ² Y	-41	ρ	207	GSB9	23 09	
152	÷	-24		208	STO4	35 04	
153	RCL5	36 05		209	STx5	35-35 05	
154	+	-55		210	P ² S	16-51	
155	RCLD	36 14		211	RTN	24	
156	X ²	53		212	*LBL9	21 09	
157	x	-35		213	X ²	53	
158	RCL2	36 02		214	x	-35	
159	x	-35		215	1	01	
160	RCL7	36 07		216	+	-55	
161	÷	-24		217	1/X	52	
162	RCLF	36 15		218	RTN	24	
163	X ²	53		219	*LBLF	21 16 15	
164	RCLD	36 14		220	P ² S	16-51	Recall K
165	X ²	53		221	RCL5	36 05	
166	-	-45		222	P ² S	16-51	
167	÷	-24		223	RTN	24	
168	CHS	-22					

LABELS					FLAGS	SET STATUS								
A	η	B	f	C	ρ	D	ε	E	P _L	0		FLAGS	TRIG	DISP
a		b		c		d		e		1		ON OFF		
0		1	B	2		3		4		2		0 ☐ ☒	DEG ☒	FIX ☒
5		6		7		8		9	P _L	3		1 ☒ ☒	GRAD ☐	SCI ☐
												2 ☐ ☒	RAD ☐	ENG ☐
												3 ☒ ☐		n <u>5</u>

Program Description I

Program Title Semi-Empirical Nuclear mass Formula

Contributor's Name Dan Shapira

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City Oak Ridge **State** Tennessee **Zip Code** 37830

Program Description, Equations, Variables A Semi Empirical formula is used to calculate approximate binding energies and mass excess for any nucleus with a given nuclear charge -Z and number of neutrons -N.

Definitions: Binding energy (B.E.) = $Z * M_p + N * M_n - M(Z,N)$
 M_p = proton mass(energy) in MeV, M_n = neutron mass in MeV
 $M(N,Z)$ = mass of nucleus having Z protons and N neutrons.
 Mass Excess = $M(Z,N) - A * \text{amu}$
 $A = Z + N$, $1\text{amu} = M(6,6)/12$ --- 1/12 mass of ^{12}C

Weizsacker's Semi-Empirical mass formula contains seven terms

$$M(Z,N) = Z * M_p + N * M_n + E_v + E_s + E_c + E_{\text{sym}} + E_{\text{pair}}$$

$$E_v = -a_1 * A, \quad E_s = a_2 * A^{2/3}, \quad E_c = a_3 * Z^2 / A^{1/3}$$

$$E_{\text{sym}} = a_4 * (Z-N)^2 / A$$

$$E_{\text{pair}} = + \text{ or } - 34 / A^{3/4} \quad \text{depending on whether Z and N are both odd or both even.}$$

$$E_{\text{pair}} = 0 \quad \text{for odd A nuclei}$$

Operating Limits and Warnings The semiempirical formula has been derived from measured masses and binding energies and is expected to work for nuclei reasonably close to the valley of stability. Usually $N \geq Z$ especially for heavier nuclei.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s) Which one of the mass-25 isobars (Nuclei with same number of protons+neutrons) is stable.

A=25 isobars are nuclei that can have N(#of neutrons) = 10, 11, 12, 13, 14 etc.
and at the same time Z(#of protons) = 15, 14, 13, 12, 11 respectively

The most stable Isobar will be the one that is most strongly bound nucleus.

The experimental observation is that the only stable Isobar of A=25 is the element Mg (Magnesium) which has Z=12 and N=13

One can make use of the semiempirical mass formula in predicting this result

For each Z and N in this group we shall calculate the binding energies (all the binding energies will be negative numbers) the largest number (in this case the most negative one) will belong to the most stable Isobar.

SOLUTION(S)	KEYSROKES	DISPLAY	COMMENTS
	10, A	10	enter Z of Isobar
	15, B	25	N of Isobar(mass displ.)
	C	-180.69	Display Binding energy
	11, A	26	new Z entered
	14, B	25	new N entered
	C	-193.53	Display binding energy
	12, A, 13, B	25	enter new Z and N
	C	-196.88	Display new binding energy
	13, A, 12, B	25	New Z, N
	C	-190.75	Display new binding energy
	14, A, 11, B	25	New Z, N
	C	-175.14	New binding energy

From the results displayed - the Z=12, N=13 combination has the highest value of binding energy.

Reference(s) De Shalit and Feshbach Theoretical Nuclear Physics

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	LBL A	31 25 11			+	61	
	STO 1	33 01			RCL 0	34 00	
	RCL 2	34 02			.	83	
	LBL 0	31 25 00		060	7	07	
	+	61			5	05	
	STO 0	33 00			Y*	35 63	
	CF 1	35 61 01			÷	81	
	F? 0	35 71 00			GSB 2	31 22 02	
	GSB 9	31 22 09			SF 1	35 51 01	
010	RTN	35 22			RTN	35 22	
	LBL B	31 25 12			LBL 2	31 25 02	
	STO 2	33 02			RCL (2)	34 24	
	RCL 1	34 01			*	71	
	GTO 0	22 00		070	RCL	35 34	
	LBL 1	31 25 01			9	09	
	F? 1	35 71 01			+	61	
	RTN	35 22			ST I	35 33	
	8	08			XCY	35 52	
	ST I	35 33			STO (2)	33 24	
020	RCL 0	34 00			RCL	35 34	
	GSB 2	31 22 02			8	08	
	RCL 1	34 01			-	51	
	GSB 2	31 22 02			ST I	35 33	
	RCL 2	34 02		080	RTN	35 22	
	GSB 2	31 22 02			LBL A	32 25 11	
	RCL 0	34 00			GSB 1	31 22 01	
	GSB 2	31 22 02			RCL A	34 11	
	RCL 0	34 00			GTO 7	22 07	
	3	03			LBL B	32 25 12	
030	1/X	35 62			GSB 1	31 22 01	
	Y*	35 63			RCL B	34 12	
	X ²	32 54			GTO 7	22 07	
	GSB 2	31 22 02			LBL C	32 25 13	
	RCL 1	34 01		090	GSB 1	31 22 01	
	X ²	32 54			RCL C	34 13	
	RCL 0	34 00			GTO 7	22 07	
	3	03			LBL d	32 25 14	
	1/X	35 62			GSB 1	31 22 01	
	Y*	35 63			RCL D	34 14	
040	÷	81			GTO 7	22 07	
	GSB 2	31 22 02			LBL e	32 25 15	
	RCL 1	34 01			GSB 1	31 22 01	
	RCL 2	34 02			RCL E	34 15	
	-	51		100	GTO 7	22 07	
	X ²	32 54			LBL C	32 25 13	
	RCL 0	34 00			GSB 1	31 22 01	
	÷	81			1	01	
	GSB 2	31 22 02			9	09	
	1	01			ST I	35 33	
050	CHS	42			GSB 4	31 22 04	
	RCL 1	34 01			GTO 7	22 07	
	Y*	35 63			LBL D	31 25 14	
	1	01			GSB 1	31 22 01	
	CHS	42		110	1	01	
	RCL 2	34 02			7	07	
	Y*	35 63			ST I	35 33	

REGISTERS									
0 A	1 Z	2 N	3	4	5	6	7	8 - a.m.u.	9 M _(P)
S0 M _(m)	S1 - a ₁	S2 a ₂	S3 a ₃	S4 a ₄	S5 - a ₅	S6	S7	S8 Z * M _p	S9 N * M _m
A E _r	B E _s	C E _c	D E _{sym}	E E _{pair}	I				

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
	GSB4	31 22 04			6	06	
	GTO7	22 07		170	GSB8	31 22 08	
	LBL E	31 25 15			1	01	
	GSB1	31 22 01			5	05	
	1	01			.	83	
	6	06			6	06	
	STI	35 33			8	08	
120	GSB4	31 22 04			CHS	42	
	LBL7	31 25 07			GSB8	31 22 08	
	RIS	34 84			1	01	
	RCL0	34 00			8	08	
	÷	81		180	.	83	
	RTN	35 22			5	05	
	LBL4	31 25 04			6	06	
	0	00			GSB8	31 22 08	
	STO6	33 06			.	83	
	LBL5	31 25 05			7	07	
130	ISZ	31 34			1	01	
	RCL	35 34			7	07	
	2	02			GSB8	31 22 08	
	5	05			2	02	
	-	51		190	8	08	
	X=0	31 51			.	83	
	GTO6	22 06			1	01	
	RCL(2)	34 24			GSB8	31 22 08	
	STO+6	33 01 06			1	01	
	GTO5	22 05			7	07	
140	LBL6	31 25 06			CHS	42	
	RCL6	34 06			GSB8	31 22 08	
	RTN	35 22			CF0	35 61 00	
	LBL9	31 25 09			RCL0	34 00	
	7	07		200	RTN	35 22	
	STI	35 33			LBL8	31 25 08	
	9	09			ISZ	31 34	
	3	03			STO(2)	33 24	
	1	01			RTN	35 22	
	.	83					
150	5	05					
	0	00					
	4	04					
	CHS	42					
	GSB8	31 22 08		210			
	9	09					
	3	03					
	8	08					
	.	83					
	7	07					
160	9	09					
	3	03					
	GSB8	31 22 08					
	9	09					
	3	03					
	9	09					
	.	83		220			
	5	05					
	7	07					
LABELS				FLAGS		SET STATUS	
A ENTER Z	B ENTER N	C B.E.	D M(Z,N)	E M. EXCESS	0 ↘	FLAGS	TRIG
a → E _v	b → E _s	c → E _c	d → E _{sym}	e → E _{par}	1 ↘	ON OFF	DISP
0 ↘	1 ↘	2 ↘	3 ↘	4 ↘	2	0 ☒ ☐	DEG ☐
5 ↘	6 ↘	7 ↘	8 ↘	9 ↘	3	1 ☒ ☐	GRAD ☐
						2 ☐ ☐	RAD ☐
						3 ☐ ☐	FIX ☐
							SCI ☒
							ENG ☐
							n 4

Program Description I

Program Title Clebsch-Gordon Coefficients and 3j Symbols Evaluation

Contributor's Name G. Richard Scott

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City Nashville

State Tennessee

Zip Code 37214

Program Description, Equations, Variables This program will evaluate all valid Clebsch-Gordon Coefficients and/or "3j" symbols coupling two states of angular momentum which are small enough so that the capacity of the calculator's factorial function is not exceeded. The fundamental formula used by the program is the Racah Formula;

$$\underbrace{\begin{pmatrix} j_1 & j_2 & J \\ m_1 & m_2 & -M \end{pmatrix}}_{3j \text{ SYMBOL}} = (-1)^{j_1-j_2+M} \sqrt{\Delta(j_1, j_2, J)} \sqrt{(j_1+m_1)!(j_1-m_1)!(j_2+m_2)!(j_2-m_2)!(J+M)!(J-M)!} \\ \times \sum_t (-1)^t \left[t!(J-j_2+t+m_1)!(J-j_1+t-m_2)!(j_1+j_2-J-t)! \right. \\ \left. \times (j_1-t-m_1)!(j_2-t+m_2)! \right]^{-1}$$

$$\text{with } \Delta(j_1, j_2, J) \equiv \frac{[(j_1+j_2-J)!(j_2+J-j_1)!(J+j_1-j_2)!]}{(j_1+j_2+J+1)!}$$

SUBJECT TO THE RESTRAINTS

$$\textcircled{1} \quad |j_1 - j_2| \leq J \leq |j_1 + j_2|$$

$$\textcircled{2} \quad m_1 + m_2 = M$$

$$\text{THE CLEBSCH-GORDON COEFFICIENT, } \langle j_1, j_2, m_1, m_2 | JM \rangle = \frac{\sqrt{2J+1}}{(-1)^{j_1-j_2+M}} \begin{pmatrix} j_1 & j_2 & J \\ m_1 & m_2 & -M \end{pmatrix}$$

Operating Limits and Warnings If any one term in the Racah formula is greater than 69, an error message will result (or else the calculator will display all 9's in the x-register). If illegitimate values are entered for j_1 , j_2 , and J or for m_1 , m_2 , and M , spurious results (ie, non-zero) may be obtained or the the calculator may get caught in a "loop" which will not terminate until the "t" value in the Racah formula exceeds 69.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s) ① SUPPOSE THE G.G. COEFFICIENT $\langle j_1 j_2 m_1 m_2 | JM \rangle$ IS NEEDED WITH $j_1 = \frac{3}{2}$, $j_2 = 2$, $J = \frac{5}{2}$; $m_1 = \frac{1}{2}$, $m_2 = 0$, $M = \frac{1}{2}$.

NOTE FOR SOLUTIONS: j_1 is "entered" by pressing "A"

j_2 " " " " B

J " " " " C

m_1 " " " " f[A]

m_2 " " " " f[B]

M is keyed in as -M and is "entered" by pressing f[C]

② IF THE 3J SYMBOL $\begin{pmatrix} j_1 & j_2 & J \\ m_1 & m_2 & -M \end{pmatrix}$ was desired, IT IS STORED IN REGISTER E.

Solution(s) ① 1.5 [A] 2 [B] 2.5 [C] .5 f[A] 0. f[B] - .5 f[C] completes entry of data

[D] starts program $\rightarrow 2.927700221-01$
(DIMENSIONLESS)

② [RCL] [E] $\rightarrow 1.195228610-01$
(DIMENSIONLESS)

Reference(s) MESSIAH, ALBERT, QUANTUM MECHANICS, VOLUME II, PP 1054-1058, NORTH-HOLLAND PUBLISHING CO. (AMSTERDAM) AND JOHN WILEY & SONS (NEW YORK), 1958.
(translated from the French edition)

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[illegible]

REGISTERS									
0	1	2	3	4	5	6	7	8	9
	USED	USED	USED	USED	USED	USED	USED	USED	USED
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
	USED	USED	USED						
A	B	C	D	E	F	G	H	I	J
USED	USED	USED	USED	32 VALUE				USED	

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STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	CLX	-51		169	+	-55	
114	SF0	16 21 00	COMPUTES	170	RCL1	36 46	
115	STOI	35 46		171	-	-45	
116	P*S	16-51	SUMMATION	172	X<0?	16-45	
117	RCL1	36 01	IN	173	GT03	22 03	
118	STOA	35 11		174	N!	16 52	
119	RCL2	36 02	RACAH	175	ST08	35 08	
120	STOB	35 12		176	CF0	16 22 00	
121	RCL3	36 03	FORMULA	177	RCL4	36 04	
122	STOC	35 13		178	RCL5	36 05	
123	P*S	16-51	(STEPS	179	RCL6	36 06	
124	*LBL2	21 02	113-198)	180	x	-35	
125	RCL3	36 03		181	x	-35	
126	RCL1	36 46		182	RCL7	36 07	
127	RCLA	36 11		183	RCL8	36 08	
128	+	-55		184	x	-35	
129	+	-55		185	x	-35	
130	RCL2	36 02		186	RCL1	36 46	
131	-	-45		187	N!	16 52	
132	X<0?	16-45		188	x	-35	
133	GT03	22 03		189	1/X	52	
134	N!	16 52		190	1	01	
135	ST04	35 04		191	CHS	-22	
136	RCL3	36 03		192	RCL1	36 46	
137	RCL1	36 46		193	Y*	31	
138	+	-55		194	x	-35	
139	RCL1	36 01		195	ST+9	35-55 09	
140	RCLB	36 12		196	ISZI	16 26 46	
141	+	-55		197	GT02	22 02	
142	-	-45		198	GT02	22 02	
143	X<0?	16-45		199	*LBL3	21 03	
144	GT03	22 03		200	ISZI	16 26 46	
145	N!	16 52		201	F0?	16 23 00	
146	ST05	35 05		202	GT02	22 02	
147	RCL1	36 01		203	RCL9	36 09	
148	RCL2	36 02		204	RCLD	36 14	
149	+	-55		205	x	-35	
150	RCL3	36 03		206	STOE	35 15	
151	RCL1	36 46		207	1	01	
152	+	-55		208	CHS	-22	
153	-	-45		209	RCL1	36 01	
154	X<0?	16-45		210	RCLC	36 13	
155	GT03	22 03		211	-	-45	
156	N!	16 52		212	RCL2	36 02	
157	ST06	35 06		213	-	-45	
158	RCL1	36 01		214	Y*	31	
159	RCL1	36 46		215	RCL3	36 03	
160	RCLA	36 11		216	2	02	
161	+	-55		217	x	-35	
162	-	-45		218	1	01	
163	X<0?	16-45		219	+	-55	
164	GT03	22 03		220	JX	54	
165	N!	16 52		221	x	-35	
166	ST07	35 07		222	RCL1	36 15	
167	RCL2	36 02		223	x	-35	
168	RCLB	36 12		224	RTN	24	

CHECKS TO
SEE IF $\frac{t}{t}$ finished;
IF SO, COMPUTES
3J VALUE,
STORES IN
REGISTER E

COMPUTES
CLEBSCH-
GORDON
COEFFICIENT

LABELS				FLAGS		SET STATUS		
A	B	C	D	E	0	FLAGS	TRIG	DISP
J ₁	J ₂	J	→ C, G		1	ON OFF		
a	m ₁	-M		e	2	0 ☒ ☐	DEG ☒	FIX ☐
0	1	2	3	4	2	1 ☐ ☒	GRAD ☐	SCI ☒
5	6	7	8	9	3	2 ☐ ☒	RAD ☐	ENG ☐
						3 ☐ ☒		n <u>9</u>

Program Description I

Program Title 32-P REMAINING ON MM.DDYYYY GIVEN MCI ON
EARLIER MM.DDYYYY
 Contributor's Name GARY G. ALTMAN
 Address 3307 NORTHBROOK DRIVE
 City MIDDLETON State WISCONSIN Zip Code 53562

Program Description, Equations, Variables

1. JULIAN DAY NUMBER IS CALCULATED AS DESCRIBED IN THE HP-67 STANDARD PAC, PAGE 04-01;
 THE NUMBER OF DAYS BETWEEN DATE 1 AND DATE 2 IS ALSO CALCULATED AS DESCRIBED IN THE HP-67 STANDARD PAC.
2. RADIOACTIVE DECAY: $(\text{INITIAL mCi})(0.5)^n = \text{mCi ON DATE 2}$, WHERE $n = 14.3 / \Delta \text{DAYS} = \text{THE NUMBER OF HALF-LIVES OF } ^{32}\text{P WHICH HAVE OCCURRED}$.
3. SUBROUTINE D YIELDS: mCi ON DATE 2 ;
 $(\text{mCi ON DATE 2})(2.2 \times 10^9 \text{ DPM}) = \text{DPM ON DATE 2}$;
 AND $(0.3)(\text{DPM}) \approx \text{CPM ON DATE 2}$
 [ASSUMES 30% COUNTING EFFICIENCY AND NO QUENCHING]
4. SUBROUTINE f C YIELDS:
 $(0.5)^n (\text{CPM ON DATE 1}) = \text{CPM ON DATE 2}$; AND
 $[(2.2 \times 10^9 \text{ DPM / mCi}) / (\text{CPM / .3})]^{-1} = \text{mCi ON DATE 2}$

Operating Limits and Warnings PROGRAM FAILS IF DATE 1 = DATE 2 OR
IF DATE 1 IS MORE RECENT THAN DATE 2.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s) 1. HOW MANY DPM (AND CPM) REMAIN OF A 0.135 mCi ^{32}P SAMPLE? GIVEN: DATE OF SPECIFIC RADIOACTIVITY RATING AS FEB 2, 1977; AND TODAY'S DATE APRIL 22, 1977.

2. HOW MANY CPM (AND mCi) REMAIN OF A 3.2×10^6 CPM SAMPLE OF ^{32}P AS MEASURED BY CHERENKOV RADIATION ON AUGUST 11, 1976?

Solution(s) 1. 2.071977 A (DISPLAY: 2443182) 4.221977 B (DISPLAY: 2443256.) C (DISPLAY: 74., THE NUMBER OF DAYS BETWEEN FEB 7 AND APR 22) 0.135 D (DISPLAY: 8.2220×10^6 , 2.466×10^6 - THE DPM AND THE CPM REMAINING)
2. 8.111976 A (2443002.) 4.221977 B (2443256.) C (254. = ΔDAYS) 3.2 EEX 6 F C (ANSWERS: 14., 2.18×10^{-8} - 14 CPM REMAINING, 2.18×10^{-8} mCi REMAINING.)

Reference(s) CALENDAR FUNCTIONS, PAGE 04-01 IN HP-67 STANDARD PAC, AND CHASE, G.D. & J.L. RABINOWITZ, PRINCIPLES OF RADIOISOTOPE METHODOLOGY, BURGESS, MINNEAPOLIS, MN (1962).

[illegible]

6: Program Listing I

67

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	F LBL A	31 25 11		57	STO 7	33 07	
2	F FIX	31 23		58	RCL A	34 11	
3	DSP 2	23 02		59	h X $\leftrightarrow$ Y	35 52	
4	RCL 4	34 04		060	RCL 6	34 06	
5	RCL C	34 13		61	X	71	
6	-	51		62	F INT	31 83	
7	3	03		63	-	51	
8	GTO 0	22 00		64	STO 6	33 08	
9	F LBL B	31 25 12		65	RCL 7	34 07	
010	RCL 3	34 03		66	1	01	
11	RCL C	34 13		67	RCL 8	34 08	
12	+	61		68	F %	31 82	
13	4	04		69	-	51	
14	F LBL 0	31 25 00		070	-	51	
15	h STO i	35 33		71	RCL 7	34 07	
16	h RV	35 53		72	1	01	
17	3	03		73	4	04	
18	6	06		74	$\div$	81	
19	5	05		75	GSB 2	31 22 02	
020	.	83		76	RCL 9	34 09	
21	2	02		77	EEX	43	
22	5	05		78	6	06	
23	STO 5	33 05		79	$\div$	81	
24	3	03		080	+	61	
25	0	00		81	DSP 6	23 06	
26	.	83		82	h RTN	35 22	
27	6	06		83	F LBL 1	31 25 01	
28	0	00		84	h RV	35 53	
29	0	00		85	$\uparrow$	41	
030	1	01		86	F INT	31 83	
31	STO 6	33 06		87	STO 7	33 07	
32	h RV	35 53		88	-	51	
33	h RV	35 53		89	EEX	43	
34	h F3?	35 71 03		090	2	02	
35	GTO 1	22 01		91	X	71	
36	h STi	33 24		92	$\uparrow$	41	
37	1	01		93	F INT	31 83	
38	2	02		94	STO 8	33 08	
39	2	02		95	-	51	
040	.	83		96	EEX	43	
41	1	01		97	4	04	
42	-	51		98	X	71	
43	RCL 5	34 05		99	STO 9	33 09	
44	$\div$	81		100	RCL 7	34 07	
45	F INT	31 83		101	1	01	
46	STO 9	33 09		102	+	61	
47	RCL 5	34 05		103	$\uparrow$	41	
48	X	71		104	h 1/X	35 62	
49	F INT	31 83		105	.	83	
050	h RCLi	34 24		106	7	07	
51	-	51		107	+	61	
52	CHS	42		108	CHS	42	
53	STO A	33 11		109	GSB 2	31 22 02	
54	RCL 6	34 06		110	RCL 6	34 06	
55	$\div$	81		111	X	71	
56	F INT	31 83		112	F INT	31 83	

REGISTERS

0	1	2	3	4	5	6	7	8	9
			DAY 1	DAY 2	365.25	30.6001	MM	DD	YYYY
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	USED	B	C	A DAYS	D	E	I	CONTROL	

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	RCL 9	34 09		169	RCL 2	34 02	
114	RCL 5	34 05		170	$\div$	81	
115	X	71		171	$h y^x$	35 63	$(\frac{1}{2})^n$
116	F INT	31 83		172	$h \frac{1}{x}$	35 62	
117	$\frac{1}{x} +$	61		173	RCL 0	34 00	
118	RCL 8	34 08		174	RCL 1	34 01	
119	$\frac{1}{x}$	61		175	X	71	
120	$h ST i$	33 24		176	X	71	
121	1	01		177	$g sci$	32 23	
122	7	07		178	DSP 4	23 04	
123	2	02		179	$f-x-$	31 84	DISPLAY DPM
124	0	00		180	$\uparrow$	41	
125	9	09		181	.	83	
126	8	08		182	3	03	
127	2	02		183	X	71	
128	$\frac{1}{x}$	61		184	$f-x-$	31 84	DISPLAY CPM
129	DSP 0	23 00		185	$h RTN$	35 22	
130	$h RTN$	35 22		186	$g 16LC$	32 25 13	
131	$f LBL 2$	31 25 02	IF INPUT TO THIS ROUTINE HAS ABS VALUE OF 1 OR >	187	$STO A$	33 11	STORE CPM
132	F INT	31 83	$Y = Y \pm 1$	188	RCL C	34 13	
133	$STO + 9$	33 61 09	$M = M \pm 12$	189	RCL 2	34 02	$\Delta DAYS = n$
134	1	01	(+ FOR PLUS INPUT)	190	$\div$	81	
135	2	02	STORE INPUT	191	.	83	
136	X	71		192	5	05	
137	-	51		193	$h x \leftrightarrow y$	35 52	
138	$h RTN$	35 22		194	$h y^x$	35 63	$(\frac{1}{2})^n$
139	$f LBL C$	31 25 13		195	RCL A	34 11	
140	DSP 0	23 00		196	X	71	
141	$STO C$	33 13		197	$f-x-$	31 84	DISPLAY CPM
142	$h F3$	35 71 03	IF INPUT FLAG TRUE, THEN STOP	198	.	83	
143	$h RTN$	35 22	COMPUTE Δ DAYS AND STOP	199	3	03	
144	RCL 4	34 04		200	$\div$	81	
145	RCL 3	34 03		201	RCL 1	34 01	
146	-	51		202	$\div$	81	
147	$STO C$	33 13		203	$h RTN$	35 22	DISPLAY mCi
148	$h RTN$	35 22					
149	$h F3$	35 71 03					
150	$STO 4$	22 04	COMPUTE Δ DAYS				
151	$f GTO C$	31 22 13					
152	DSP 1	23 01	STORE CONSTANTS				
153	$f LBL D$	31 25 14					
154	$STO 0$	33 00					
155	1	01					
156	4	04					
157	.	83					
158	3	03					
159	$STO 2$	33 02					
160	2	02					
161	.	83					
162	2	02					
163	EEX	43					
164	9	09					
165	$STO 1$	33 01					
166	$f LBL E$	31 25 15	$\Delta DAYS = n$				
167	2	02	14.3				
168	RCL C	34 13					

LABELS				FLAGS		SET STATUS												
A	DATE 1	B	DATE 2	C	Δ DAYS	D	mCi $\rightarrow$ CPM	E		0		FLAGS		TRIG		DISP		
a		b		c	CPM $\rightarrow$ mCi	d		e		1		ON	OFF			VARIES		
0	CALC	1		2		3		4		2		0	☐	☒	DEG	☒	FIX	☐
5		6		7		8		9		3	INPUT	1	☐	☒	GRAD	☐	SCI	☐
												2	☐	☒	RAD	☐	ENG	☐
												3	☐	☒			n	

NOTES

NOTES

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