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## NAVAL POSTGRADUATE SCHOOL Monterey, California

## POSITION DETERMINATION WITH <br> LORAN-C TRIPLETS AND THE HEWLETT-PACKARD HP-67/97 PROGRAMMABLE CALCULATORS

by
R. H. Shudde

March 1980

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Prepared for:
Chief of Naval Research
Arlington, Virginia 22217

## NAVAL POSTGRADUATE SCHOOL MONTEREY, CALIFORNIA

Rear Admiral J. J. Ekelund
Jack R. Boasting Superintendent Provost

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This report presents an algorithm and HP-67/97 programs for position determination with Loran-C chains. Operational data cards are prepared in advance for Loran-C triplets. Position determination is performed using a single program card and an appropriate operational data card.

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## by

R. H. Shudde

Naval Postgraduate School Monterey, California

March 1980


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## ABSTRACT

This report presents an algorithm and HP-67/97 programs for position determination with Loran-C chains. Operational data cards are prepared in advance for Loran-C triplets. Position determination is performed using a single program card and an appropriate operational data card.

## A. Introduction

The Loran system is a radio aid to navigation which utilizes the principle of hyperbolic fixing. The locus of points for which the difference in arrival time of synchronized signals from a pair of transmitters is constant determines a hyperbolic line of positions (LOP). The intersection of two hyperbolic lines of position from two pairs of transmitters determines position or a hyperbolic fix. That two pairs of stations are required for a fix does not necessarily mean that there are four separate stations, for one station of one pair may be colocated with one station of the other pair forming a Loran triplet (Figure 1). Triplets may be joined "end-to-end" by station colocation to form a Loran chain (Figure 2). Loran chains are common on both the East and West Coasts of the North American continent.

The early "Standard Loran" or Loran-A" operating at a frequency just below 2 MHz is still in use in the Pacific area. The present day "Loran-C" operates at $100-\mathrm{kHz}$ and is in use in both the Atlantic and Pacific Areas. The computational algorithm and programs described herein can be used for position determination with Loran-C triplets. Further information on the history, development and operation of the Loran systems may be found in References 1 and 2.

(a) Colocated Master Stations

(b) Colocated Slave Stations

(c) Colocated Master and Slave

Figure 1. Loran Triplets.
2


Figure 2. Loran Chain of Five Loran Triplets.

## B. Program Description

One program card and one operational data card (described below) are all that is required for on-location position determination from Loran triplet time-difference measurements. Two program cards are required to prepare operational data cards; these operational data cards should be prepared and validated prior to on-location navigational use. Thus although three program cards are described only one program card is required for navigation; two program cards are used to prepare operational data cards during or prior to mission planning. The function of each program card and its intended use follows.

Program Card 1. This program card is used to prepare master data cards. A master data card requires the following information for a master (M) station/slave(S) station pair:

1. A M/S pair identification number.
2. The quantity $\Delta t$ which is the sum of the coding delay plus the one way base line time in microseconds.
3. The latitude and longitude of the master station.
4. The latitude and longitude of the slave station.

Some preprocessing of these data is performed before the master data card is generated. The data generated require only one side of an HP-67/97 magnetic card for each M/S pair, thus a second M/S pair may be placed on side 2 of the card (thus conserving cards) if desired. It is envisaged that a master data card will be prepared in advance for each $M / S$ pair that might be received within an area of operation.

Program Card 2. This program card is used to prepare an operational data card for every Loran triplet within an operational area. Each operational data card contains data merged from the master data cards which contain $M / S$ pair information for each pair of the triplet. These merged data are validity checked, colocation of master or slave determined and encoded.

The only inputs required for this program are the two master data cards that comprise the Loran triplet. It is possible to prepare and store operational data cards rather than master data cards. This may be desirable if there is no scarcity of cards and storage space, however the number of possible Loran triplets is considerably larger than the number of $M / S$ pairs.

Program Card 3. This program card is used in conjunction with an operational data card for position determination. Required input is the indicated time difference $T$ for each M/S pair of the triplet. Output is the computed latitude and longitude of the fix. Note: Every Loran fix has two possible solutions. The unwanted solution can almost always be rejected by inspection, however, if the stations of the Loran triplet are nearly aligned then either solution may be valid even though only one solution should be consistent with the flight plan.

## C. HP-67/97 Calculator Programs

1. User Instructions

CARD 1

| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Read in program card (both sides) |  |  |  |
| 2. | Input a unique ID number for the Loran pair* | ID | f a | ID |
| 3. | Input the coding delay $\Delta t$ | $\Delta t$ | f C | $\Delta t$ |
| 4 a b. | Input the master station latitude and longitude (CHS for West)** | $\begin{aligned} & \phi_{M} \\ & \lambda_{M} \end{aligned}$ | $\stackrel{\uparrow}{\text { A }}$ | --- |
| $5 a$. b. | Input the slave station latitude and longitude (CHS for West) | $\begin{aligned} & \$ s \\ & \lambda_{s} \end{aligned}$ | $\begin{aligned} & \uparrow \\ & c \end{aligned}$ | ---- |
| 6 a b. | Run <br> Pass a blank data card through the card reader. | None | E | crd |
|  | The format for position data input is of the form: $\pm$ DDD.MMSSFF, where <br> DDD denotes degrees <br> MMM denotes minutes <br> SS denotes seconds <br> FF dnotes hundredths of a second. <br> The minus sign (-) denotes Southern latitudes or Western longitudes. |  |  |  |


| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Read in program card 2 |  | E |  |
| 2a. | Start | --- |  | 9.00 |
| b. | 9.00 will flash in the display. Insert a master data card containing the first pair of a Loran triplet. |  |  |  |
| c. | 9.00 will flash in the display once more. Insert a master data card containing the second pair of the Loran triplet. |  |  | 9.00 |
| d. | If the data form a proper triplet, "crd" will appear in the display. |  |  | crd |
| e. | Pass both sides of a blank card thru the card reader to produce the operational data card for the Loran triplet. |  |  |  |
|  | Should "error" appear in the display, then the two master data cards do not compare to form a Loran triplet. Both the latitude and longitude of the colocated stations must be identical on both master data cards in order to successfully produce an operational data card. |  |  |  |

Label the A key position with the identification number of the first Loran pair (the pair inserted in Step $2 b$ ) and label the $B$ key position with the identification number of the second Loran pair (from Step 2c).

| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Read in both sides of the program card 3. |  |  |  |
| 2. | Read both sides of the operational data card for the Loran triplet that you are receiving. |  |  |  |
| 3 a . | Set to compute Solution A. |  | f a | --- |
| b. | Set to compute Solution B. |  | f b | --- |
| 4. | Input the observed time delay from the first Loran pair. | T | A | --- |
| 5. | Input the observed time delay from the second Loran pair. | T | B | --- |
| 6. | Compute fixLatitude <br> Longitude |  | $\begin{aligned} & E \\ & R / S \end{aligned}$ | Latitude Longitude |
| 7. | Repeat from Step 2 with a new operational data card or from steps 3 or 4 as required. |  |  |  |

CARD 1

| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | In this series of examples we will prepare and use data cards for the Loran-C pairs 9930X and 9930Y. <br> Read in program card 1 (both sides) |  |  |  |
| 2. | Input the ID for 9930x | 9930.1 | f a | 9930.10 |
| 3. | Input the coding delay $\Delta t$ for 9930X | 36389.66 | f c | 36389.66 |
| 4 a b. | Input the master station <br> latitude <br> and longitude (CHS for West) | $\begin{array}{r} 34.034604 \\ -77.544676 \end{array}$ |  | --- |
| 5 a. b. | Input the slave station latitude and longitude (CHS for West) | $\begin{array}{r} 46.463218 \\ -53.102816 \end{array}$ | $\begin{aligned} & \uparrow \\ & c \end{aligned}$ | --- |
| 6 a. b. | Compute <br> Pass a blank data card through the card reader. Label the card 9930X MASTER | None | E | crd |
| 7. | Input the ID for 9930 Y | 9930.2 | f a | 9930.2 |
| 8. | Input the coding delay $\Delta t$ for 9930Y | 52541.31 | $\mathrm{f} \quad \mathrm{c}$ | 52541.31 |
| $9 a$. b. | Input the master station <br> latitude <br> and longitude (CHS for West) | $\begin{array}{r} 34.034604 \\ -77.544676 \end{array}$ | $\begin{aligned} & \uparrow \\ & A \end{aligned}$ | --- |
| 10a. | Input the slave station <br> latitude <br> and longitude (CHS for West) | $\begin{array}{r} 41.151193 \\ -69.583909 \end{array}$ | $\begin{aligned} & \uparrow \\ & \mathrm{C} \end{aligned}$ | ---- |
| 11a. <br> b. | Compute <br> Pass a blank data card (or the second side of the card used in Step 6b) through the card reader. Label the side $9930 Y$ MASTER | None | E | crd |
| 12. | These twn cards will be used in the next example. |  |  |  |


| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Read in program card 2. |  |  |  |
| 2a. | Start | --- | E | 9.00 |
| b. | While 9.00 is flashing in the display, insert the MASTER data card for station 9930X into the card reader. |  |  |  |
| c. | When 9.00 starts flashing in the display again, insert the MASTER data card for station $9930 Y$ into the card reader. | --- |  | 9.00 |
| d. | "Crd' will appear in the display. | --- |  | crd |
| e. | Pass both sides of a blank card through the card reader. <br> Label this card 9930X/9930Y OPERATIONAL DATA CARD. Then label the $A$ key position $9990 x$ and the $B$ key position 9930 . This card will be used in the next example. | --- |  | 0.00 |

CARD 3

| Step | Instructions | Input Data/Units | Keys | Output Data/Units |
| :---: | :---: | :---: | :---: | :---: |
| 1. | You are receiving 9930X and 9930Y and wish to obtain a fix. <br> Read in program card 3 (both sides) |  |  | --- |
| 2. | Read in the operational data card for the triplet $9930 X / 9930 Y$ (both sides) |  |  | --- |
| 3. | Select Solution A. |  | $f \quad \mathrm{a}$ |  |
| 4. | The indicated time delay is $49400 \mu \mathrm{~s}$ from 9930y. <br> Input the indicated time delay. | 49400 | B | 0.00 |
| 5. | The indicated time delay is 28800 us from 9930x. <br> Input the indicated time delay. | 28800 | A | 0.00 |
| 6. | Solution A: 420 $44^{\prime} 57{ }^{\prime \prime} \mathrm{N}$ Latitude $41^{\circ} 07^{\prime} 32^{\prime \prime}$ W Lonqitude |  | $\begin{aligned} & \mathrm{E} \\ & \mathrm{R} / \mathrm{S} \end{aligned}$ | $\begin{array}{r} 42.4457 \\ -41.0732 \end{array}$ |
|  | $\left\{\begin{array}{l} \text { Solution B: } 27^{\circ} 00^{\prime} 07^{\prime \prime} \text { S Latitude } \\ 102^{\circ} 27^{\prime} 12^{\prime \prime} \mathrm{E} \text { Longitude } \\ \text { Since you are navigating over } \\ \text { the North Atlantic, Solution A } \\ \text { is the desired fix. } \end{array}\right\}$ |  |  |  |
| 7. | Repeat from Step 2 with a new operational data card or from Steps 3 or 4 as required. |  |  |  |

3. Program Storage Allocations and Program Listings

Card 1.

## Registers:

R0: ID
Rl: $\Delta t$
R2: 2c
R3:
R4: ${ }^{\theta} \mathrm{M}$
R5: ${ }^{\lambda} M$
R6: ${ }^{\varepsilon}$ MS
R7: ${ }^{6} S$
R8: $\lambda_{S}$
R9: ${ }^{\varepsilon_{S M}}$

SO: L
Sl: T
S2: U
S3: V
S4: X
S5: $\quad \mathbf{Y}$
S6: $\quad \delta_{1} d$
s7: $\Delta \lambda_{\mathrm{m}}^{\prime}$
S8: d
S9: f

Initial Flag Status and Use:

| $0:$ | OFF, Unused | 2: OFF, Unused |
| :--- | :--- | :--- |
| $1:$ | OFF, Unused | 3: |

Display Status:
DSP 4, FIX, DEG.

## User Control Keys:

$\mathrm{A}: \quad \quad_{\mathbf{M}}{ }^{\uparrow} \lambda_{\mathbf{M}}$
a: Station ID
B:
b:
C: ${ }^{\phi} S^{+1}{ }^{\lambda} S$
c: $\Delta t$
D:
d:
E: Prepare data card
e:

## Card 2.

Registers:

| R0: | $\pm \mathrm{ID}_{1}$ | so: | $\pm \mathrm{ID}_{2}$ | RA: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R1: | $\Delta t_{1}$ | S1: | $\Delta t_{2}$ | RB: |  |
| R2: | $2 \mathrm{c}_{1}$ | s2: | $2 \mathrm{C}_{2}$ | RC: |  |
| R3: |  | S3: |  | RD: |  |
| R4: | ${ }^{\text {Al }}$ | S4: | ${ }^{\text {A2 }}$ | RE: | $a_{p}=21295.87$ |
| R5: | $\lambda_{\text {Al }}$ | S5: | $\lambda_{\text {A2 }}$ | RI: | $f=1 / 298.26$ |
| R6: | ${ }^{\text {A }}$ Al | S6: | $\xi_{\text {A2 }}$ |  |  |
| R7: | $\theta_{\text {Bl }}$ | S7: | ${ }^{\text {B }}$ 2 |  |  |
| R8: | $\lambda_{B 1}$ | S8: | $\lambda_{B 2}$ |  |  |
| R9: | $\xi_{B 1}$ | S9: | $\xi_{B 2}$ |  |  |

Initial Flag Status and Use:
0: OFF, Vertex determination
2: OFF, Validity checking
1: OFF, Unused
3: OFF, Unused

## Display Status:

DSP 2, FIX, DEG

User Control Keys:
A:
a:
B:
b:
C:
c:
D:
d:
$E: \quad$ Run
e:

## Card 3.

Registers:

| R0: | $\mathrm{ID}_{1}$ | S0: | $\mathrm{ID}_{2}$ | RA: | M |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R1: | $\Delta t_{1}$ | S1: | $\Delta t_{2}$ | RB: | $\mathrm{u}, \mathrm{N}$ |
| R2: | (2c) ${ }_{1}$ | S2: | $(2 \mathrm{c})_{2}$ | RC: | D, d |
| R3: | $\mathrm{A}_{1}, \mathrm{c}_{2}, \mathrm{P}$ | S3: | $\mathrm{A}_{2}$ | RD: | $\Delta \sigma$ |
| R4: | $\theta_{1}=\theta_{F}$ | S4: | ${ }^{*}$ | RE: | $a_{p}=21295.87$ |
| R5: | $\lambda_{1}=\lambda_{F}$ | S5: | $\lambda_{2}$ | RF: | $\mathrm{f}=1 / 298.26$ |
| R6: | $\xi_{1}$ | S6: | $\xi_{2}$ |  |  |
| R7: | $\mathrm{c}_{1}, \mathrm{c}_{1}, \mathrm{H}$ | S7: | $\mathrm{C}_{2}$ |  |  |
| R8: | $B_{1}, S / a=r$ | S8: | $\mathrm{B}_{2}$ |  |  |
| R9: | $a_{1}$ | S9: |  |  |  |

Initial Flag Status and Use:
0: OFF, Soln A, Soln B
1: OFF, Unused
2: OFF, M/S Vertex Flag
3: OFF, Unused

Display Status:
DSP 2, FIX, DEG

User Control Keys:
A: $\mathrm{T}_{1}$
a: Soln $A$
B: $\mathrm{T}_{2}$
b: Soln B
C:
c:
D:
d:
E: Run
e:

14

| Ce： | UE： | $\therefore$ it $\therefore$ ： | Store | 039 | －LELE | 21 15 | Main Routine：Renewal Solution |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 485 | c－ib | 可 6 | Station ID． | 045 | FCL4 | 3684 |  |
| E： 5 | FTN | Ei |  | 841 | RLL 7 | 36 E\％ | Compute and／or |
| 084 | －EEC | 2116 iz |  | 04.3 | $+$ | －55 | store： |
| 80： | $5 \times 1$ | T5 E1 | Store $\Delta$ t． | 045 | 2 | 82 |  |
| 80 | FTN | $E 4$ |  | 044 | $\div$ | －24 |  |
| E日， | HELH | ＜1： | Store longitude | 845 | STG6 | 3513 | $\theta_{m}=\left(\theta_{1}+\theta_{2}\right) / 2$ |
| gils | H！ | $16 \pm$ | Store longitude | 046 | PCLi | 3667 |  |
| Oベこ | 5165 | 35135 | and store parametric latitude | 047 | RCL4 | 3684 |  |
| 010 | EEE | 2302 | of the master station． | 046 | － | －45 |  |
| 611 | $\therefore T 14$ | 3544 | Of the master station． | 049 | 2 | 02 |  |
| 012 | FTN | 24 |  | $00^{6}$ | $\div$ | －24 |  |
| $0 \cdot 3$ | 1LELC | $21: 3$ |  | 651 | STG0 | 3514 | $\Delta \theta_{m}=\left(\theta_{2}-\theta_{1}\right) / 2$ |
| 014 |  | $10^{\circ} 5$ | Store longitude and | 852 | RCL8 | 36 EC | m 2 |
| 815 | ST5 | 350 |  | 853 | FEL5 | 3605 |  |
| 016 | 6S69 | $2 \overline{3}$ | store parametric latitude | 6． $0^{4}$ | － | $-45$ |  |
| 615 | 5767 | 3517 | of the slave station． | 055 | STOE | $3515$ | $\Delta \lambda=\lambda_{2}-\lambda_{1}$ |
| Q18 | FTN | 24 |  | 65 | $2$ | $02$ | $\lambda_{2} 1$ |
| 019 | －LEL9 | 21 ¢ |  | （2） | $\div$ | －24 |  |
| 0 ET | $\because$ | $16^{-41}$ |  | 058 | STEI | 3540 | $\Delta \lambda_{m}=\Delta \lambda / 2$ |
| $00_{1}$ | HHE＊ | 1632 | Subroutine to | 059 | F＊S | 16－5i | m |
| 025 | TAN | 43 | convert | E60 | RCLO | 3614 |  |
| 025 | 1 | 01 | convert | 86.1 | COS | 42 |  |
| 0.4 | ENT1 | －i | geographic（geodetic） | $8 E 2$ | 只 | 55 | $H=\cos ^{2} \Delta \theta_{m}-\sin ^{2} \theta$ |
| ES | i | 82 | latitude to | E03 | RCLC | 3613 | $\mathrm{m} \quad \mathrm{~m}$ |
| $\because 5$ | 9 | 89 | latitude to | 00.4 | SIH | 41 |  |
| 627 | 6 | 62 | parametric latitude． | $6 E .5$ | X2 | 53 |  |
| 050 | － | －62 | parametric latitude． | 866 | － | －45 |  |
| 日こ〇 | 2 | 03 |  | 867 | RCLI | 3640 |  |
| 038 | 6 | EE |  | ． 868 | SIH | $4 i$ |  |
| 031 | $1 \times$ | E |  | 609 | $x^{2}$ | 52 |  |
| 032 | F－S | $10^{-5} 5$ |  | ©08 | $\therefore$ | －35 |  |
| 053 | ET09 | 3542 | Store flattening | （1） | KCLO | $36: 4$ |  |
|  |  | 16－5： | constant． | ¢iz | SIN | － 41 |  |
| 0.35 | － | －45 | constant． | 073 | X2 | 53 |  |
| 0.36 | TAM | $10-35$ |  | 0.74 |  | －55 |  |
| 037 938 | TAN－ RTN | 1643 |  | 075 | 9700 | 35 00 | $L=\sin ^{2} \Delta \theta_{m}+H \sin ^{2} \Delta \lambda_{m}$ |
| 038 | RTN | $6^{4}$ |  | 076 | ENTT | －21 |  |


| E, | + | - -5 |  | 115 | flis | 36 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.8 | i | $\because:$ |  | 110 | Fils | 3005 |  |
| $0^{-2}$ | - | -4 |  | 117 | 年 | -45 |  |
| 68\% | -45 | -i |  | 115 | 5005 | 35 | $\mathrm{Y}=\mathrm{u}-\mathrm{V}$ |
| 0 O | C5-4 | 15: |  | 115 | Ins | - - |  |
| $69 ?$ | cris | 350 | $d=\cos ^{-1}(1-2 L)$ | 129 | KCli | 364 |  |
| 605 | jata | 1645 |  | $1: 1$ | FiLi | 36 E |  |
| 084 | LS\% | 10-6\% |  | 12 | $\stackrel{ }{ }$ | -55 |  |
| ces | EId | 41 |  | 123 | + | -55 |  |
| 856 | $\div$ | -i4 |  | 124 | RCL9 | 306 |  |
| 88, | $5 T 01$ | 3581 | $\mathrm{T}=\mathrm{d} / \mathrm{sin} \mathrm{d}$ | 125 | A | - |  |
| cis | FiLic | $36:$ |  | 120 | 4 | $0 \cdot$ |  |
| ceo | SIN | i: |  | 12 | $\div$ | -̇i |  |
| 090 | FCLI | $3 \mathrm{E}: 4$ |  | 128 | 5700 | 356 | $\delta_{1} \mathrm{~d}=\mathrm{f}(\mathrm{TX}-\mathrm{Y}) / 4$ |
| ect | cas | 45 |  | 129 | Chis | -23 | ${ }_{1}{ }^{\text {a }}=\mathrm{I}(\mathrm{X}$ |
| 832 | $\times$ | -35 |  | 136 | RCLJ | 3601 |  |
| $00 ?$ | xi | 5 |  | 121 | - | -55 |  |
| 69.4 | ENT: | -21 |  | 122 |  | 3608 |  |
| 0.35 | ${ }^{+}$ | - E5 |  | 15 | SIH | 41 |  |
| 680 | ! | U: |  | 12.4 | - | -35 |  |
| 09-1 | Kil | JE 0 |  | 135 | F-5 | 1098 |  |
| 00s | - | -45 |  | 130 | F:5 | 1t-51 |  |
| 090 | $\stackrel{\square}{5}$ | -i9 |  | 15 | STJE | 350 |  |
| 106 | ST0̇ | 350 | $U=2 \sin ^{2} \theta_{m} \cos ^{2} L \theta_{\mathrm{m}} /(1-L)$ | 138 | F\%S | it-5: | $2 \mathrm{c}=\mathrm{S} / \mathrm{a}_{\mathrm{e}}=\left(\mathrm{T}-\delta_{1} \mathrm{~d}\right)$ sin $d$ |
| 101 | FこL | J̄E it | m m ${ }^{\text {m }}$ | 159 | PCL5 | 3505 |  |
| $10 ?$ | SIN | 46 ! |  | 140 | RCL 8 | 36 - |  |
| 183 | $\mathrm{FCLL}_{6}$ | 3612 |  | 141 | ENT ${ }^{1}$ | - : ! |  |
| $10:$ | 695 | İ |  | 142 | $+$ | -55 |  |
| 195 | $\therefore$ | $\because$ |  | 143 | 1 | E! |  |
| 100 | $\therefore 2$ | 5 |  | 144 | - | -45 |  |
| 187 | ERIT? | -2: |  | 145 | 4 | E: |  |
| 188 | + | -E5 |  | 146 | RCL4 | 30.44 |  |
| 105 | FCLG | Jte 0 |  | 147 | - | -4E |  |
| 110 | $\stackrel{\square}{\square}$ | -24 |  | 148 | $x$ | -35 |  |
| 111 | ¢T03 | 3505 | $\mathrm{V}=2 \sin ^{2} \Delta \theta_{m} \cos ^{2} \theta_{m} / L$ | 149 | + | -55 | $F / 2=[Y-(1-2 L)(4-X)]$ |
| 112 | kCL2 | 3608 |  | 150 | RCLS | 3602 |  |
| 113 | $\stackrel{+}{\text { STO4 }}$ | -55 |  | 151 | RCLI | 36 Cl | -2G = fT |
| 114 | ST04 | 3504 | $\mathrm{X}=\mathrm{U}+\mathrm{V}$ | 152 | x | -35 | $-2 \mathrm{G}=\mathrm{PT}$ |



Subroutine
Exchange storage of
master and slave station
is at the vertex of the
triplet.
Change sign of the ID
to signal that the slave
station is at the triplet
vertex.
Subroutine
Dtation of one pair is co-
located with the slave
station of the other pair.
Rearrange data and set
f2 if a colocation is
found.

号




| $\alpha=\gamma+\cos ^{-1}(\kappa / \rho)$ | 115 |  | -65 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 116 | - | -45 |  |
| Store $\alpha$ | 117 | ; | -1 |  |
|  | 118 | ${ }^{+}$ | -55 |  |
|  | 119 | 5706 | 3515 | $\mathrm{D}=1-2 \mathrm{c}_{2}-\mathrm{c}_{1} \mathrm{M}$ |
|  | 150 | 1: | 52 |  |
|  | 121 | 5123 | 35-35 $\mathbf{6}^{3}$ |  |
|  | 122 | FCLS | 呺 | $P=\mathrm{C}_{2} / \mathrm{D}$ |
|  | 123 | $\stackrel{\mathrm{KCl}}{\substack{\text { c }}}$ | 30 |  |
|  | 125 | STL | 3515 | $\mathrm{d}=\mathrm{s} /(\mathrm{ad}$ ) |
|  | 126 | RCL4 | 3664 | $\mathrm{d}=\mathrm{s} /\left(\mathrm{a} \mathrm{e}^{\mathrm{D})}\right.$ |
| $r=\operatorname{qatn}\left[\frac{B_{i}}{C_{i} \cos \left(\alpha-\xi_{i}\right)+A_{i}}\right]$ | 127 | : | - |  |
|  | 128 | $+$ | 84 |  |
|  | 130 | cos | 36 4 |  |
|  | 131 | \% | -35 |  |
|  | 132 | \% | -i |  |
|  | 133 | +F | 34 | $\sigma_{1}=q \operatorname{tatn}\left(N, \sin \theta_{1}\right)$ |
| $\mathrm{M}=\cos \theta_{1} \sin \alpha_{12}$ | 134 | Ci: | -51 |  |
|  | 135 | RCi | 3613 |  |
| where $\alpha_{12}=\xi_{1}$ | 135 | - | -i5 |  |
| Where 12 | 137 189 | $y^{2}$ | - $\begin{array}{r}05 \\ -95\end{array}$ |  |
| $c_{1}=f M$ | 139 | STES | 3512 | $u=2\left(\sigma_{1}-\mathrm{d}\right)$ |
|  | 140 | Cos | $4{ }^{2}$ | $\square_{1}$ |
|  | 141 | - | 0 |  |
|  | 142 | $\checkmark$ | -as |  |
|  | 143 | kici | 36 |  |
|  | 144 | $\therefore$ | -35 |  |
|  | 145 | CHS | -28 |  |
| $c_{2}=f\left(1-M^{2}\right) / 4$ | 146 147 | $\pm$ | - |  |
|  | 147 148 | KCL | 50-5 |  |
|  | 149 | RCIS | 3013 | $W=1-2 p \cos u$ |
|  | 150 | $\stackrel{+}{+}$ | -55 |  |
|  | 151 | cos | 4 | $v=\cos (u+d)$ |
|  | $15 \%$ | $\because$ | -35 |  |






D. Loran-C Fixing Algorithms

The development of the Loran fixing algorithms in this report is presented in more detail in a companion report [Ref. 3] and will not be repeated here.

The basic Loran-C equation [Ref. 4] can be written as

$$
\begin{equation*}
T=\left[T_{S}+p\left(T_{S}\right)\right]-\left[T_{M}+p\left(T_{M}\right)\right]+\left[T_{B}+p\left(T_{N}\right)\right]+\delta \tag{1}
\end{equation*}
$$

where
$T$ is the "indicated time difference" in microseconds, $T_{M}, T_{S}$ is the distance, in microseconds, from the master and the slave to the receiver, respectively,
$T_{B}$ is the distance, in microseconds, between the master and the slave,
$\delta$ is the assigned coding delay, in microseconds, and $p(T)$ is the secondary phase correction, in microseconds, for an all sea water path of length $T$.

The quantity

$$
\wedge_{t}=\left[T_{B}+p\left(T_{B}\right)\right]+\delta
$$

is a constant for each master/slave pair. The following World Geodetic System 1972 (WGS 72) values have been adopted for Loran-C navigation [Ref. 4]:

$$
\begin{aligned}
v_{0}= & 299792458 \text { meters/second is the velocity of light } \\
& \text { in free space, } \\
\eta= & 1.000338 \text { is the index of refraction of the surface } \\
& \text { of the earth for standard atmosphere and } 100 \mathrm{kHz} \\
& \text { electromagentic waves, } \\
a_{e}= & 6378135.00 \text { meters is the equatorial radius of the } \\
& \text { earth, and } \\
f= & 1 / 298.26 \text { is the flattening factor }\left(1-b / a e^{\prime}\right. \text { where } \\
& b \text { is the polar radius) of the earth. }
\end{aligned}
$$

Accurate formulas for computing the secondary phase correction $p(T)$ are contained in Reference 4 , but for use with the handheld calculator the following linear approximation [Ref. 3] will be used:

$$
p(T)=a_{1}+a_{2} T
$$

where
and

$$
\begin{aligned}
& a_{1}=-0.321 \\
& a_{2}=0.000635
\end{aligned}
$$

Using this approximation, it is possible to solve Equation 1 for the quantity $T_{S}-T_{M}$. We find

$$
\begin{equation*}
T_{S}-T_{M}=(T-\Delta t) /\left(1+a_{2}\right) \tag{2}
\end{equation*}
$$

On the surface of a sphere a hyperbolic line of position can be represented by the equation [Ref. 3, page 175]

$$
\begin{equation*}
\tan r=\frac{\cos 2 a-\cos 2 c}{\sin 2 c \cos \omega+\zeta \sin 2 a} \tag{3}
\end{equation*}
$$

where the origin of the coordinate system is at the prime focus of the spherical hyperbola, 2 c is the spherical arc joining the foci, 2a is a constant for any one LOP, and $r$ and $\omega$ are the spherical coordinates of a point on the LOP. If the base line of the coordinate system is the arc joining the foci then $\omega$ is the spherical polar angle from the base line to a point $P$ on the LOP and $r$ is the spherical polar distance (or arc) from the prime focus to $P$. Using the Loran system we take $\zeta=+1$ if the prime focus is at a master station and we take $\zeta=-1$ if the prime focus is at a slave station. If we take $v=v_{0} / \eta$ to be the velocity of 100 kHz electromagnetic radiation of the earth's surface then

$$
2 a=v\left(T_{S}-T_{M}\right) / a_{e}
$$

or, using Eq. (2),

$$
\begin{equation*}
2 a=(T-\Delta t) / a_{p} \tag{4}
\end{equation*}
$$

where

$$
a_{p}=\frac{a_{e}\left(1+a_{2}\right)}{v_{0} / \eta}=21295.87 \mu \mathrm{~s}
$$

The baseline between master and slave can be obtained from

$$
\begin{equation*}
2 c=v T_{B} / a_{e} \tag{5}
\end{equation*}
$$

Here 2 c is computed by program card 1 (preparation of master data cards) using the algorithm in Section $E$.

Consider a Loran-C triplet with master stations colocated. Let $\xi_{1}$ and $\xi_{2}$ denote the azimuth angles of slave $1\left(S_{1}\right)$ and slave $2\left(S_{2}\right)$, respectively, measured from North toward the East from the master stations (M) (see Fig. 3). Further, let $\alpha$ and $r$ denote the azimuth and spherical polar arc (distance) of the receiver (R) from M. For this geometry, Eq. (3) can be written as

$$
\begin{equation*}
\tan r_{i}=\frac{B_{i}}{C_{i} \cos \left(\alpha-\xi_{i}\right)+A_{i}} \tag{6}
\end{equation*}
$$

where

$$
\begin{aligned}
& A_{i}=\zeta_{i} \sin 2 a_{i} \\
& B_{i}=\cos 2 a_{i}-\cos 2 c_{i}
\end{aligned}
$$

and

$$
c_{i}=\sin 2 c_{i}
$$

for the $i=$ th Loran pair, $i=1,2$. Since $r=r_{1}=r_{2}$, tan $r_{i}$ can be eliminated in Eq. (6). The resulting equation can be rewritten as

$$
\begin{equation*}
C \cos \alpha+S \sin \alpha=K \tag{7}
\end{equation*}
$$

where

$$
\begin{aligned}
& C=B_{1} C_{2} \cos \xi_{2}-B_{2} C_{1} \cos \xi_{1} \\
& S=B_{1} C_{2} \sin \xi_{2}-B_{2} C_{1} \sin \xi_{1} \\
& \kappa=B_{2} A_{1}-B_{1} A_{2} .
\end{aligned}
$$

and


Figure 3. Geometry of a Loran Triplet and a Receiver.

## If we define $\beta>0$ and $\gamma$ by the equations

and

$$
\begin{align*}
& \rho \cos \gamma=C, \\
& \rho \sin \gamma=S, \tag{8}
\end{align*}
$$

then

$$
\beta=\sqrt{c^{2}+s^{2}}
$$

and

$$
\gamma=\operatorname{qatn}(S, C)
$$

Here the function qatn $(y, x)$ is the arctangent of $y / x$ adjusted for the proper quadrant according to the signs of $x$ and y. A compact form of this function is

$$
\operatorname{qatn}(y, x)=\tan ^{-1} \frac{y}{x+10^{-9} t(x=0 ?)}+\pi t(x<0 ?)
$$

where

$$
t(z)=1 \text { when } z \text { is true }
$$

and

$$
t(z)=0 \text { when } z \text { is false. }
$$

When convenient we will use the notation qatn(y/x) interchangeably with qatn $(y, x)$. The qatn function is equivalent to the polar angle obtained using the rectangular to polar conversion function on the HP-67/97.

Now substitute Eq. (8) into Eq. (7) and solve for

$$
\begin{equation*}
\alpha=y \pm \cos ^{-1}(\kappa / \beta) \tag{9}
\end{equation*}
$$

to obtain the azimuth angle $\alpha$ of the two points of intersection of the LOP's. Finally we obtain a value for $r$ by substituting each $\alpha$ into Eq. (5). We find that

$$
r=\operatorname{qatn}\left[\frac{B_{i}}{C_{i} \cos \left(\alpha-\xi_{i}\right)+A_{i}}\right] \quad \text { for } i=1 \text { or } 2
$$

The distance and azimuth from $M$ or the triplet vertex can be converted into the latitude and longitude of the two possible positions of $R$.

The fixing algorithm then uses $\alpha$ and $r$ in the direct. solution algorithm of spheroidal geodesy (Section F).

## E. The Reverse (Inverse) Solution Algorithm

This reverse solution algorithm is a modification of the first order in flattening (f) algorithm given by Thomas [Ref. 5, pp. 8-101. Thomas' notation has been followed as closely as possible for ease of comparison of the algorithms. The gatn function is defined in Section D. West longitudes ( $\lambda$ ) and South latitudes (1) are negative. We are given the points $P_{1}\left(:_{1},{ }_{1}\right), P_{2}\left(\Phi_{2}, \lambda_{2}\right)$ on the spheroid and are to find the distance $S$ between the points and the forward and back azimuths, ${ }^{12}$ and ${ }^{2} 2_{1}$. Given quantities are $\Phi_{1}, \lambda_{1}{ }^{\prime} \$_{2}$ and ${ }_{2}$. No assumptions about the relative location of $P_{1}$ and $P_{2}$ are required. The modified mo..rrir solution algorithm is:

$$
-1 i,+41) 4, \quad \therefore \frac{1}{m}(\therefore+() \quad \therefore
$$

$$
\begin{aligned}
& i_{i}=\tan ^{-1}\left[(1-f) \tan \phi_{i}\right], \quad i=1,2 . \\
& { }_{m}=\left(\cdot_{1}+4_{2}\right) / 2, \quad \therefore H_{m}=\left(\theta_{2}-\cdot \cdot_{1}\right) / 2, \quad \therefore i=1_{2}-\lambda_{1} \text {, }
\end{aligned}
$$

$$
\begin{aligned}
& \text { 1. }-\sin ^{2} \therefore \mu_{m}+H \sin ^{2} \therefore_{m}=\sin ^{2}(d / 2), 1-L=\cos ^{2}(d / 2) \text {, } \\
& { }^{-1}(1-2 L), U=2 \sin ^{2} \operatorname{mos}^{2} \cdot \cos ^{\prime}(1-L), \\
& V . \quad \therefore 1 n^{2} \therefore \cos ^{2} \quad n+1, x=u+v, Y=u-v, \\
& \text { : in } 4,{ }_{1}^{d}=f(T X-Y) / 4, S=a_{t}\left(T-i{ }^{d}\right) \sin d, \\
& \because Y-(1-2 L)(4-X) 1, \quad ;=f T / 2,
\end{aligned}
$$

$$
\begin{aligned}
& t_{1}=q \tan \left(-\sin \Delta \theta_{m} \cos \Delta \lambda_{m^{\prime}}^{\prime} \cos \theta_{m} \sin \Delta \lambda_{m}^{\prime}\right), \\
& t_{2}=q \tan \left(\cos \Delta \theta_{m} \cos \Delta \lambda_{m^{\prime}}^{\prime} \sin \theta_{m} \sin \Delta \lambda_{m}^{\prime}\right), \\
& \alpha_{12}=t_{1}+t_{2}, \alpha_{21}=t_{1}-t_{2} .
\end{aligned}
$$

This reverse solution algorithm is used by program card 1 (preparation of master data cards) to compute the baseline distance $2 c$ and the azimuths $\xi_{M S}$ and ${ }^{\xi_{3}}$ SM between the master and slave stations of a Loran pair.

Details of the modifications made to Thomas' algorithm are contained in Reference 3.

## F. The Direct Solution Algorithm

This direct solution algorithm is a modification of the first order in flattening (f) algorithm given by Thomas [Ref. 5, pp. 7-8]. Thomas' notation has been followed as closely as possible for ease of comparison of the algorithms. The qatn function is defined in Section $D$. West longitudes and South latitudes are negative. We are given the point $P_{1}\left(\phi_{1}, \lambda_{1}\right)$ on the spherioid, where $\phi_{1}, \lambda_{1}$ are the geodetic latitude and longtiude (geographic coordinates); the forward azimuth ${ }^{\alpha}{ }_{12}$ and the distance $S$ to a second point $P_{2}\left(\phi_{2}, \lambda_{2}\right)$; and from these we are to find the geographic coordinates $\phi_{2}{ }^{\prime} \lambda_{2}$ and the back azimuth ${ }^{\alpha}{ }_{21}$. The given quantities are '1' ' 1 ' ' 12 and $S$. No assumptions about the relative location of $P_{1}$ and $P_{2}$ are required. The modified direct solution algorithm is:

$$
\begin{aligned}
& \left.\theta_{1}=\tan ^{-1}((1-f) \tan )_{1}\right], \quad M=\cos \theta_{1} \sin \alpha_{12} \\
& \mathrm{~N}=\cos \mathrm{c}_{1} \cos \alpha_{12}, \quad c_{1}=\mathrm{fm}, \quad c_{2}=\mathrm{f}\left(1-\mathrm{m}^{2}\right) / 4, \\
& D=1-2 c_{2}-c_{1} M, \quad P=c_{2} / D, \quad \sigma_{1}=\left(\operatorname{atn}\left(N, \sin \theta_{1}\right)\right. \\
& d=s /\left(a_{e} D\right), \quad u=2\left(i_{1}-d\right), \quad w=1-2 P \cos u, \\
& V=\cos (u+d), \quad Y=2 P V W \sin d, \quad \Delta \sigma=d-Y, \\
& { }_{21}=\operatorname{tath}\left[-M,-\left(N \cos \alpha-\sin \theta_{1} \sin \Lambda(\theta)\right),\right. \\
& K=(1-f)\left(M^{2}+\left(N \cos \therefore-\sin { }_{1} \sin \Delta(y)^{2}\right)^{1 / 2}\right. \text {. } \\
& t_{,}=\tan ^{-1} \mid\left(\sin { }_{1} \cos A+N \sin (n) / k \mid\right. \text {, }
\end{aligned}
$$

This direct solution algorithm is used by program card 3 (improved fix program) to compute the latitude and longitude of the receiver using the azimuth and range of the receiver from the Loran triplet vertex.

Details of the modifications made to Thomas' algorithm are contained in Reference 3.

## G. Discussion and Some Typical Results

## The HP-67 program design specifications of

COMPATWINGSPAC [Ref. 6] are contained in the following statement.
"There is a need for an HP-67 program that will compute a geographical position from two Loran delay rate readings. Several methodoloqies are available to compute the desired position but computational complexities increase with the desired accuracy and flexibility. The most desirable accuracy would be an error of less than $4 \mathrm{n} . \mathrm{ms}$. at a range of $500 \mathrm{n} . \mathrm{mi}$. Wili less error closer to the. stations. It is likely that program length considerations will require that the station pairs have a common site (i.e. two slaves or two masters at the same location). This is not an unusual situation as evidenced by strings of station pairs along coast lines. A data card will probably be necessary for the station pairs to be used. However, more than one program card is unacceptable due to the decrease in functional utility when compared to the manual plotting method. As a final requirement, the fix should be obtainable on either side of the baselines connerting the stations, and not limited to a geometric position relative to one side or the other of the stations."

It was further stated that the maximum computation time to obtain a fix be 1.5 minutes.

It is felt that these design goals have been satisfied. Although one program is required to prepare master data cards for all Loran-C pairs and a second card is required to prepare
operational data cards, one each for every triplet, this preparation should be done only once. The data cards should be supplied to users verified and labeled, by the Fleet Mission Program Library. One program card and an appropriate operational data card are all that is required for the fixing algorithm.

The fixing algorithm will display one of the two possible receiver positions in 38 seconds following the entry of the time delay readings. Since there are situations in which either of the two solutions could be the valid solution; the decision of which solution to use should be left to the operator, not the program designer.

Testing of the algorithm for all Loran-C triplets and positions relative to those triplets was too extensive a program to be carried out in the available time. Some "typical" scenarios however are presented in Tables I through IV. As can be seen all errors are all well within the design specifications of $4 \mathrm{n} . \mathrm{mi}$ at $500 \mathrm{n} . \mathrm{mi}$ range from the stations. The time delay values in these Tables were generated using a program discussed in Reference 3. It is recommended that the $\mathrm{P}-3$ community test the algorithm for accuracy in known areas of operation and examine the results for possible regions in which the algorithm may fall outside the design requirements. Such testing shoild be compatible with the known "unreliable regions" shown on the Loran-C charts.

Table I. Moffett Field South

| Position |  | Indicated Time Delay |  | Fix |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lat | Long | 9940x | 9940Y | Lat (N) | Long (W) | n.mi |
| $24^{\circ} \mathrm{N}$ | $122{ }^{\circ} \mathrm{W}$ | 27726.19 | 40912.76 | 23059'55" | $122^{\circ} 00^{\prime} 01^{\prime \prime}$ | 0.08 |
| 26 | 122 | 27715.97 | 40998.39 | 25*59'57' | $122^{\circ} 00^{\prime} 01^{\prime \prime}$ | 0.05 |
| 28 | 122 | 27702.41 | 41117.84 | 2759'59" | $122^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.02 |
| 30 | 122 | 27683.53 | 41291.85 | 29*59'59" | $122^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.02 |
| 32 | 122 | 27655.47 | 41555.46 | $32^{\circ} 00^{\prime} 00^{\prime \prime}$ | 122"00'00" | 0.00 |
| 34 | 122 | 27609.63 | 41959.57 | $34^{\circ} 00^{\prime} 00^{\prime \prime}$ | $122^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 36 | 122 | 27523.56 | 42544.11 | $36^{\circ} 00^{\prime} 00^{\prime \prime}$ | 121*59'59" | 0.01 |
| 38 | 122 | 27334.61 | 43248.22 | $38^{\circ} 00^{\prime} 00^{\prime \prime}$ | 121*59'58' | 0.03 |

Table II. Moffett Field West

| Position |  | Indicated Time Delay |  | Fix |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lat | Long | 9940Y | 9940w | Lat (N) | Long (W) | $\mathrm{n} . \mathrm{mi}$ |
| $37^{\circ} \mathrm{N}$ | $122^{\circ} \mathrm{W}$ | 42892.86 | 16257.23 | 36*59'59' | $122^{\circ} 00^{\prime} 01^{\prime \prime}$ | 0.02 |
| 37 | 125 | 43056.68 | 15765.13 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $125^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 37 | 128 | 43137.78 | 15327.12 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $128^{\circ} 00^{\circ} 00^{\prime \prime}$ | 0.00 |
| 37 | 131 | 43191.10 | 14970.77 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $131^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 37 | 134 | 43232.38 | 14683.74 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $134^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 37 | 137 | 43267.42 | 14449.40 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $137^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 37 | 140 | 43298.80 | 14254.02 | $37^{\circ} 00^{\prime} 00^{\prime \prime}$ | $140^{\circ} 00^{\prime} 01^{\prime \prime}$ | 0.01 |
| 37 | 143 | 43327.85 | 14087.43 | $37^{\circ} 00^{\prime} 01^{\prime \prime}$ | 142*59'59' | 0.02 |

Table III. Brunswick Northeast

| Position |  | Indicated Time Delay |  | Fix |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lat | Long | 79302 | 9930x | Lat (N) | Long (W) | n.mi |
| $60^{\circ} \mathrm{N}$ | $30^{\circ} \mathrm{W}$ | 52437.86 | 28451.72 | 6000'03" | 2959'32' | 0.24 |
| 58 | 35 | 51960.93 | 28391. 50 | 58 ${ }^{\circ} 00^{\prime} 00^{\prime \prime}$ | 34* ${ }^{\circ} 9^{\prime} 46^{\prime \prime}$ | 0.11 |
| 56 | 40 | 50992.37 | 28359.15 | 55*59'59" | 3959'54" | 0.06 |
| 54 | 45 | 49292.46 | 28370.85 | 53*59'59" | 4459'57' | 0.03 |
| 52 | 50 | 47165.60 | 28490.64 | $52^{\circ} 00^{\prime} 00^{\prime \prime}$ | 4959'59" | 0.01 |
| 50 | 55 | 45236.59 | 29070.48 | $50^{\circ} 00^{\prime} 00^{\prime \prime}$ | $55^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 48 | 60 | 44505.60 | 30991.94 | $48^{\circ} 00^{\prime} 00^{\prime \prime}$ | $60^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 46 | 65 | 44475.70 | 33697. 14 | $46^{\circ} 00^{\prime} 00^{\prime \prime}$ | $65^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.00 |
| 44 | 70 | 44588.91 | 36567.42 | $43^{\circ} 59^{\prime} 59^{\prime \prime}$ | $69^{\circ} 59^{\circ} 59^{\prime \prime}$ | 0.02 |

Table IV. Jacksonville Southeast

| Position |  | Indicated Time Delay |  | Fix |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lat | Long | 9930W | 9930x | Lat (N) | Long (W) | $\mathrm{n} . \mathrm{mi}$ |
| $9^{\circ} \mathrm{N}$ | $47^{\circ} \mathrm{W}$ | 13058.04 | 36466.46 | 859'19" | 46*59'22" | 0.92 |
| 12 | 52 | 12984.71 | 37288. 35 | 11*59'34" | 515 ${ }^{\circ}{ }^{\prime \prime}{ }^{\prime \prime}$ | 0.57 |
| 15 | 57 | 12898.73 | 38267. 58 | 14*59'44" | 5659'47' | 0.34 |
| 18 | 62 | 12793.91 | 39431.32 | 17059'52" | 61*59'54" | 0.16 |
| 21 | 67 | 12656.52 | 40794. 36 | 2059'56" | 66059'57" | 0.08 |
| 24 | 72 | 12451.30 | 42330.55 | 23*59'59" | 71059'59" | 0.02 |
| 27 | 77 | 12097.12 | 43876. 62 | 27*00'01" | $77^{\circ} 00^{\prime} 00^{\prime \prime}$ | 0.02 |
| 30 | 82 | 12973.95 | 44768. 53 | $30^{\circ} 00^{\prime} 01 \prime$ | $82^{\circ} 00^{\prime} 06^{\prime \prime}$ | 0.09 |

H. References

1. J. A. Pierce, A. A. McKenzie, and R. H. Woodward, editors, LORAN, M.I.T. Radiation Laboratory Series, McGraw-Hill Book Company, Inc., 1948.
2. G. Hefley, The ievelopment of Loran-C Navigation and Timing, National Bureau of Standards Monograph 129, U. S. Department of Commerce, U. S. Government Printing Office, Washington, D.C. 20402, October 1972.
3. R. H. Shudde, "An Algorithm for Position Determination Using Loran-C Triplets with a BASIC Program for the Commodore 2001 Microcomputer," Technical Report NPS55-80-009, March 1980, Naval Postgraduate School, Monterey, CA 93940 .
4. LORAN HYPERBOLIC LOP FORMULAS AND GENERAL SPECIFICATIONS FOR LORAN-C (20 June 1949) were obtained from G. R. Young, Acting Chief, Navigation Department, Defense Mapping Agency, Hydrographic/Topographic Center, Washington, D.C. by private communication, 5 March 1980.
5. Paul D. Thomas, "Spheroidal Geodesics, Reference Systems, and Local Geometry," SP-138, U. S. Naval Oceanographic Office, Washington, D.C., January 1970.
6. Private communication from COMPATWINGSPAC representatives, Moffett Field, CA., October 1979.

## APPENDIX. Loran-C Station Parameters

The following list contains the pertinent parameters for each Loran-C station pair. This list was compiled from data in Reference 4. Each column contains the following information:

1. The Loran-C station pair designator
2. $\Delta t$, the sum of the coding delay plus one way baseline time, including the secondary phase correction for an all seawater path, in microseconds.
3. The master station latitude.
4. The master station longitude.
5. The slave station latitude.
6. The slave station longitude.

In this list, negative longitudes are West and positive longitudes are East. If desired, this convention may be reversed since the algoxithms are independent of such external conventions; if this is done, care should be taken that the signs of all longitudes in the list are reversed. In columns 3 through 6 the latitudes and longitudes appear to be in decimal form, but the actual format is DDD.MMSSFF (which is compatible with the $\mathrm{HP}-67 / 97 \mathrm{H} . \mathrm{MS}$ input mode) where

DDD designates degrees,
MM designates minutes,
SS designates seconds, and
FF designates hundredths of seconds.


| Station | Location |
| :--- | :--- |
| 4990 | Central Pacific |
| 5930 | East Coast, Canada |
| 5990 | West Coast, Canada |
| 7930 | North Atlantic |
| 7960 | Gulf of Alaska |
| 7970 | Norwegian Sea |
| 7980 | Mediterranean Sea |
| 7990 | Great Lakes |
| 8970 | East Coast, U.S.A. |
| 9930 | West Coast, U.S.A. |
| 9940 | Northeast U.S.A. |
| 9960 | Northwest Pacific |
| 9970 | North Pacific |
| 9990 |  |

## Station

4990
5930
5990
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Location
Central Pacific
East Coast, Canada
West Coast, Canada
North Atlantic

Gulf of Alaska
Norwegian Sea

Southeast U.S.A.
Mediterranean Sea

Great Lakes
East Coast, U.S.A.

West Coast, U.S.A.
Northeast U.S.A.

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Dean of Research, Code 012 ..... 1
Naval Postgraduatr SchoolMonterey, CA 93940
Office of Naval Research ..... 2
Fleet Activity Support DivisionCode ONR-2 30800 North Quincy Street
Arlington, VA 22217
Attn: Mr. Robert Miller
Office of Nival pesearch ..... 1
Code ONR-434
800 Nor: $: ~ Q u i n c y ~ S t r e e t$
Arlington, VA 22217
Navy Tactical Support Activity ..... 2P.O. BOX ? 04t
Silver Soriags, MD ..... 20910
COMPATWIVGSPAC ..... 4Naval Air Station
Moffet: Fin:l, Cr ..... 94035
Attn: Codu 5l and Code 532
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Attn: Code N7
COMFATWI:OG ELE:VR: TSC NAS ..... 1
Jacksonville, FL 32212
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Commanding Officer
Air Test and Evaluation Squadron 1 (VX-1)
Patuxent River. MD 20670
Attn: Code 713
Commanding Officer
Submarine Development Group Two Groton, CT 06340

Director 1
Strategic Systems Project Office
1931 Jefferson Davis Highway
Arlington, VA 20376
Attn: Code SP2021
Naval Air Development Center Johnsville, FA 18974
Attn: Code 2022
Center for Naval Allalysis
1401 Wilson Boulevird
Arlington, VA 222 (19
Attn: Greg Watson
Naval Weapons Laboratory
Dahlgren, VA 22443
Naval Weapons Center
1
China Lake, CA $93: 555$
Naval Surface Weapons Center
1
White Oak
Silver Spring, MD 20910
Naval Research Laboratory
1
Washington, D.C. 20390
David Taylor Naval Ship Research
and Development Center
Bethesda, MD 20034
Naval Ocean Systcms Center 1
San Diego, CA 92132
Naval Intelligence Support Center
4301 Suitland Foad
Washincton, D.C. 20390
Naval Electronics Systems Command 1 2511 Jeffersun Duvis lighway Arlington, $V$ N 20360
Naval Underwater Systems Center ..... 1
Code Sis 3
New Lonion, CT 06320
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Hyattsville, MD 20782
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Washington, D.C. ..... 20361
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Newport. Phode Islaid 02840
Naval Oranance Station ..... 1
Indian Head, MD 20;40
Naval Surface Weapois Center ..... 1
Dahlgren, VA 22448
Anti-Sutmarine Warfare Systems Project Office ..... 1
Department of the Navy Washington, D.C. 20360
Attn: Code ASW-137
Surface Warfare Development Group ..... 2
Naval Amehibious Base
Little Cresk, VA 23511
Attn: Code N32 and C. Cartledge
combuscramme ..... 1
Norfolk, rA 23511
Attn: Code :Vil2
Deput $\because$ Comsunder ..... 1
Operatirna! rist and Evaluation Force Pacific
NAS : Uorth Island
San Diaco. Ca.vp-241NAS
Jacksonville, FL 32212
Attn: ituc ficnrath D. Walker

Assistant Wing TAC D\&E Officer
ASW Operations Department
NAS
Cecil Ficld, FL 32215
Attn: Code vS-24

Naval Electromagnetic Spectrum Center

Naval Communications Unit
Washington, D.C. 20390

Attn: CDR Claude I aVurre

VS-Support Unit
NAS
Cecil Field, FI, 32215
Attn: CWO Wentworth
1 ROCAL-Codt 18
Fleet kuadiness Office
NOSC
San Dicao, CA 92152
Attn: Jim Grant
Chief of Naval Matericl I
MAT 0GDl
Departmont of the Nave
Washincton, r.C. ? 0360
Attn: CuR prilip Harvey
LT Jan Smith
1
COMCRUDESGRU TWO
FPO New York, NY 09501
Dr. Thomas Burnett 1
Dept. of Management Science
OR Study Group
U.S. Naval Academy

Annapolis, MD 21401
U. S. Naval Oceanoqraphic office

1
Washington, D.C. 20309
Attn: Paul D. Thomas
Naviaration Department
1
Defonse Mapping Agency Hydrographic Topographic center Washiniton, D.C. 20315
Attn: G. R. DeyoungL'T Michael D. Redshaw1
Helicopter Antisubmarine Squadron ..... 7
FPO New York 09501
Mr. Raymond F. Fish ..... 1Naval Underwater Systems CenterNewport, RI 02840
LT Kenneth W. Peters ..... 1
Commanding Officer
U. S. Naval Air Facility APO New York 09406
LT Peter W. Marzluff ..... 1Surface Warfare Officer's SchoolNewport, RI 02840
L'T Ray C. Pilcher, Jr.1Surface Warfare Officer's SchoolNiwport, RI 02840
LT William M. Yerkes ..... 1
ASWOC NAF
S'qonella Sicily
Flo New York 09523
LiT A. J. Kocirey1CommanderCruiser-Destroyer Group Two
FPO New York 09501
LCDR E. G. Schwier1
USS Estocin (FFG 15)
FPO New York 09501
LCOER. R. Hillyer ..... 1Code N3llCommander, Carrier Group FourF'po New York 09501
ICDR J. W. Pattison1Code N 321
Commander, Carrier Group Eight
Pru New York 09501
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ASWCC NAF LAJES
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AP() New York 09523
LT R. N. Christianson ..... 1
ASW
Naval Postgraduate School
Monterey, CA 93940
LT L. R. Erazo ..... 1
ASWOC SIGONELLA
FPO New York 09523
LT R. E. Springman ..... 1
USS Lexington (ANT-16)
Naval Air Station
Pensacola, FL 32504
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Patrol Squadron 26
Special Project Det
Naval Air Station
Brunswick, ME 04011
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FPO New York ..... 09501
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USS John F. Kennedy (CU-67)
FPO New York ..... 09501
LCDR Michael A. Santoro ..... 1
Air Antisubron 41
NAS North Island
San Diego, CA 92135
LCDR Robert M. Hanson ..... 1
Helasron Four
NAS North Island
San Diego, CA ..... 92135
LT Michael D. Thomas ..... 1
2476 Ridgecrest Ave.Orange Park, FL 32073
LT Carl E. Garrett, Jr. ..... 1
Class 65, Dept. Head Course
Surface Warfare School, Naval BaseNewport, RI 0284047Naval Postgraduate SchoolMonterey, CA 93940
Attn: Prof. R. N. Forrest, Code 55Fo ..... 1
Prof. R. H. Shudde, Code 55Su ..... 200R. J. Stampfel, Code 551
LT M. D. Clary1
USS PAIUTE (ATF-159)
FPO New York 09501


